

# Asymmetric collapse by dissolution or melting in a uniform flow

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An advection–diffusion–limited dissolution model of an object being eroded by a two-dimensional potential flow is presented. By taking advantage of the conformal invariance of the model, a numerical method is introduced that tracks the evolution of the object boundary in terms of a time-dependent Laurent series. Simulations of a variety of dissolving objects are shown, which shrink and then collapse to a single point in finite time. The simulations reveal a surprising exact relationship whereby the collapse point is the root of a non-analytic function given in terms of the flow velocity and the Laurent series coefficients describing the initial shape. This result is subsequently derived using residue calculus. The structure of the non-analytic function is examined for three different test cases, and a practical approach to determine the collapse point using a generalized Newton–Raphson root-finding algorithm is outlined. These examples also illustrate the possibility that the model breaks down in finite time prior to complete collapse, due to a topological singularity, as the dissolving boundary overlaps itself rather than breaking up into multiple domains (analogous to droplet pinch-off in fluid mechanics). In summary, the model raises fundamental mathematical questions about broken symmetries in finite-time singularities of both continuous and stochastic dynamical systems.

## I. INTRODUCTION

Interfacial growth processes, such as alloy solidification [1–4], electrodeposition [5, 6], and crystal formation [7, 8], are responsible for a wide variety of complex natural patterns [9, 10] that emerge due to instabilities in the underlying equations for interface motion [11, 12]. Often, continuum models of interfacial growth exhibit finite-time singularities, whereby features of the interface, such as curvature, diverge after finite time. The formation of such singularities is indicative of a breakdown in the separation of scales between the macroscopic variables in the continuum model and the microscopic variables that have been ignored [13, 14]. In fluid mechanics, the presence of finite-time singularities has been extensively studied, and can frequently provide physical insight [15], such as identifying the existence of universal scaling behavior in the pinch-off of a column of fluid [16, 17].

A particularly good example of interfacial growth is diffusion-limited aggregation (DLA) [18], where a solid cluster of particles is grown from a bath of diffusing particles starting from a single static seed particle. Additional particles are introduced one by one far away from the cluster, carry out random walks until they adhere to the cluster upon contact, causing it to grow. Since a random walker is more likely to first meet an extremity of the cluster than an interior region, the extremities grow preferentially, leading to complex fractal clusters in discrete computer simulations of the model [18–21].

Growth processes related to diffusion-limited aggregation have also been studied in the continuum limit, whereby the steady-state walker concentration satisfies Laplace’s equation

outside the cluster, is zero on the cluster boundary, and tends to a steady concentration far away from the cluster, and the cluster boundary grows continuously and deterministically with its velocity proportional to the normal gradient of the diffusing concentration field. This limit is mathematically equivalent to the classical Saffman–Taylor problem [22] of viscous fingering in a Hele–Shaw cell without surface tension [23, 24]. This model is conformally invariant, which simplifies the analysis and allows it to be studied in detail in two dimensions using conformal mapping [25], as first formulated in 1945 by Polubarinova-Kochina [26, 27] and Galin [28] for applications to oil recovery and water filtration in porous media. Continuous diffusion-limited growth is notoriously unstable, and perturbations in an object’s boundary progressively sharpen, eventually leading to the formation of cusps in finite time [29–31]. In viscous fingering, these finite-time singularities are regularized by surface tension [24, 32, 33], which leads instead to tip branching instabilities and the formation of fractal fingering patterns [23].

Hybrid discrete–continuous models have also been developed based on iterated conformal maps [34], which take full advantage of conformal invariance in two dimensions [25]. The growing cluster is defined by a chain of conformal maps that each add a small bump to the shape to represent the aggregation of a single particle, which opens new possibilities, such as growing non-random, fractal clusters [31]. By studying the statistics of the stochastic conformal map, it can also be shown that the average shape of random DLA clusters is similar [35], but not identical [36, 37], to the corresponding shape of continuous, deterministic diffusion-limited growth.

Both the stochastic and continuous growth models have been extended to allow for any gradient-driven transport process in two dimensions [38], on flat or curved surfaces [39], which is made possible by a general conformal invariance princi-

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ple [40]. In the canonical case of advection-diffusion-limited aggregation (ADLA) of random walkers in a fluid potential flow, asymptotic approximations of the flux profile have been studied [41], and the discrete and continuous cases have been compared [37]. These studies of ADLA provide the motivation for the present work.

In this paper, we consider when the sign of growth is switched in the ADLA model, corresponding to dissolution or erosion: we start with a solid object, and then random walkers in a flow annihilate small parts of it on contact. Even in the absence of flow, this case has received much less investigation, since it usually leads to stable dynamics [21, 35, 42, 43] and thus many of the complex patterns due to growth instabilities are no longer manifest. However, this model opens up alternative questions for study. In a previous paper [44], several different conformally invariant transport-limited dissolution models were introduced, including the erosion of corrugations on an infinite surface, and the expansion of a cavity due to dissolution. The paper also introduced the system of advection-diffusion-limited dissolution (ADLD), whereby an object is dissolved due to a concentration of random walkers in a fluid potential flow past the object. The object is represented by a time-dependent conformal map from the unit circle to the physical domain. By making use of previous asymptotic results [41], an evolution equation for the conformal map is derived for the regime of intermediate Péclet number. The mathematical model is similar to the model of freezing and melting of dendrites in a hydrodynamic flow considered by Kornev and coworkers [45–47], where the random walker concentration field in our model is replaced by a temperature field governed by an advection-diffusion equation. However, these works use a different mathematical formulation, employing the Schwarz function [48] to model the time-dependent boundary, and consider a different model for interfacial motion.

The previous study of ADLD [44] was entirely analytical, and thus only considered the simple shapes of a circle and ellipse. Here, we investigate this model in more depth, and develop a numerical implementation that can simulate the dissolution of arbitrarily shaped objects. By simulating arbitrary objects, we are able to investigate the model in substantially more mathematical detail, particularly in relation to the formation of several different types of finite-time singularity.

### A. Physical applications of the model

While the model that we consider is for a mathematically idealized two-dimensional case, it is worth considering what situations it could be applied to. For free gas or liquid flow, the model is unlikely to apply. Laminar flow at high Reynolds number  $Re$  can be approximated as a potential flow with viscous boundary layer of width  $1/\sqrt{Re}$ , but our model assumes that the diffusion layer of width  $1/\sqrt{Pe}$ , which is much wider than any viscous boundary layer for the regime of intermediate Péclet number that we consider. For melting, this would imply a small Prandtl number  $Pr$ , while for dissolution this would imply a small Schmidt number  $Sc = Pe/Re$ . However, for most liquids  $Sc \gg Pr \gg 1$ , since momentum diffuses much more

rapidly than heat or mass. For gases,  $Sc \sim Pr \sim 1$  since the same collisional mechanism governs mass, momentum, and heat transfer, but this still violates the model assumptions since the viscous and diffusion boundary layers would have similar size.

One area where the model may apply is for dissolution or two-phase flow in porous media, which has relevance to water transport in soils or to flow in oil reservoirs, as in the seminal papers [26–28]. In this case, the fluid can be modeled using Darcy flow, and the object would represent a solidified region within the porous medium undergoing dissolution or melting (as considered by Kornev and coworkers [45–47]). A similar model of nonlinear advection-diffusion in a potential flow is also applicable to viscous gravity currents in Hele-Shaw cells or porous-media flows, in which a heavier fluid spreads diffusively by gravity on an impermeable surface, as it is sheared by the flow of a lighter fluid above it [49]. The model could also have applications to a variety of different electrochemical corrosion processes [50–52], whenever a flow is imposed to modify the diffusive transport of active ionic species.

The model may also be relevant to dissolution driven by electrokinetic phenomena, in the regime where double layers are thin in comparison to the object size. Consider a fixed object that is uniformly charged, in a fluid that is driven by a uniform electric field. In this case the fluid motion will be well-modeled by a potential flow where the electric potential is proportional to the fluid potential. The model could also apply to an object moving via electrophoresis. An object of constant surface charge will move at a constant speed in a uniform electric field, regardless of its shape [53], and hence constant flow at infinity could be fictitious flow of a stagnant fluid in a frame of reference of a particle moving at constant velocity by electrophoresis as it dissolves.

The model we consider is in a substantially different regime than recent experiments and simulations of the erosion of clay bodies in high Reynolds number fluid flows [54], where the erosion rate of the surface is proportional to shear stress, and the dissolving bodies tend towards a self-similar cone-like shape [55].

### B. Layout of the paper

The paper proceeds as follows. In Section II, we present the theoretical background of the model, and derive an evolution equation for the shape of a dissolving body in terms of a time-dependent conformal map from the unit circle to the physical domain, described by a Laurent series. In Section III, we then derive a system of ordinary differential equations that govern how the Laurent series coefficients evolve with time. We numerically integrate this system using an eighth-order timestepping method [56, 57], which allows the dissolution process to be simulated very accurately, close to the limit of machine precision.

Our initial numerical results for a variety of objects show that they completely dissolve in a finite duration with their boundaries becoming progressively smoother (Section IV). As

expected, the flow causes the objects to dissolve more quickly on the side facing upstream, although the details of the process are complicated, and affected by the precise manner that the fluid flows past the dissolving object. Of particular interest is the location of the collapse point, where the dissolving object finally vanishes. Due to the high accuracy of our simulations, we inferred an exact relationship between the collapse point  $z_c$  expressed as a complex number, the speed of the flow, and the initial Laurent coefficients. The relationship is surprising, whereby  $z_c$  is the root of a non-analytic function  $P$ , the terms of which involve complicated products of Laurent series terms. While some of these terms share similarities with binomial and multinomial expansions, they are distinctly different, and we are unaware of any other problem in conformal mapping or elsewhere where they occur.

In Section V we make use of residue calculus to derive the general form of  $P$ , using the numerical results as a guide. The complicated products of terms in  $P$  arise from the residue of a contour integral where several Laurent series are multiplied together. In general, the function  $P$  has multiple roots, thus creating ambiguity about which root is the collapse point, and in Section VI we consider three different example objects that highlight the structure of  $P$  in more detail. To find the roots of  $P$ , we introduce a generalized Newton–Raphson iteration. As usual for Newton–Raphson iterations, plots of the root convergence in terms of the initial starting guess are fractal, but the non-analyticity of  $P$  creates some distinct morphological differences, and the plots illustrate the difficulties of determining the collapse point with mathematical certainty.

The three examples also exhibit several types of finite-time singularity, which are both physically relevant and provide insight into the mathematical well-posedness of the model. Connections between these singularities and  $P$  are discussed. While the dissolution model that we consider is a simplified model with stable dynamics, it has a surprising amount of mathematical structure, and our results raise a number of questions for further study.

## II. THEORETICAL BACKGROUND

We make use of non-dimensionalized units, and consider an object in two dimensions with a time-dependent boundary  $S(t)$  as shown in Fig. 1(a). The object is immersed in an inviscid, irrotational fluid with velocity  $\mathbf{v}(\mathbf{x}, t)$ , which can be written in terms of a potential  $\phi(\mathbf{x}, t)$  as  $\mathbf{v} = \nabla\phi$ . The fluid is incompressible, so  $\nabla \cdot \mathbf{v} = 0$  and hence

$$\nabla^2\phi = 0. \quad (1)$$

At the boundary of the object the condition  $\hat{\mathbf{n}} \cdot \mathbf{v} = \hat{\mathbf{n}} \cdot \nabla\phi = 0$  is used, where  $\hat{\mathbf{n}}$  is an outward-pointing normal vector. Far away from the object the flow tends to a constant horizontal velocity so that  $\mathbf{v}(\mathbf{x}, t) \rightarrow (1, 0)$  as  $|\mathbf{x}| \rightarrow \infty$ . Equivalently, the potential satisfies  $\phi(\mathbf{x}, t) \rightarrow x$  as  $|\mathbf{x}| \rightarrow \infty$ .

The fluid transports a random walker concentration  $c(\mathbf{x}, t)$  that satisfies the advection–diffusion equation

$$\text{Pe}\nabla c \cdot \nabla\phi = \nabla^2 c, \quad (2)$$

where  $\text{Pe}$  is the Péclet number, a dimensionless quantity describing the ratio of advection to diffusion. Far away from the object, the random walker concentration tends to unity, so that  $c(\mathbf{x}, t) \rightarrow 1$  as  $|\mathbf{x}| \rightarrow \infty$ . The random walkers are responsible for dissolving the object. At the boundary of the object,  $c(\mathbf{x}, 0) = 0$ . The normal velocity of the object boundary  $S(t)$  is given by

$$\sigma = -\lambda \hat{\mathbf{n}} \cdot \nabla c, \quad (3)$$

where  $\lambda$  is a dimensionless constant. Equations (1) and (2) together with the associated boundary conditions form a closed system for  $(\phi, c, S)$  that describe the dissolution dynamics, but they are difficult to solve directly. To proceed, we therefore treat the object as being in the complex  $z$  plane, where  $z = x + iy$ , and we introduce a time-dependent conformal map described by an analytic function  $z = g(w, t)$  that transforms the unit circle  $C$  into the object boundary  $S(t)$ , as shown in Figure 1(b). The most general form of the conformal map is the truncated Laurent series,

$$g(w, t) = a(t)w + \sum_{n=0}^N q_n(t)w^{-n}, \quad (4)$$

where  $a(t)$  is taken to be a real function, and  $q_n(t)$  are complex functions. Hereafter, we refer to  $q_n$  as the  $n$ th mode. Both Eqs. (1) and (2) are conformally invariant. The Laplacian is the standard example of a conformally invariant operator, and the advective term  $\nabla c \cdot \nabla\phi$  is also conformally invariant [38, 40].

The boundary conditions in the  $w$  plane are different. Due to the scaling factor  $a(t)$  in Eq. (4), the boundary condition on the velocity potential becomes  $\phi(w, t) \rightarrow a\text{Re}(w)$  as  $|w| \rightarrow \infty$ . We therefore introduce a rescaled potential  $\hat{\phi}(w, t) = \phi(w, t)/a$  that satisfies the original boundary condition  $\hat{\phi}(w, t) \rightarrow \text{Re}(w)$  as  $|w| \rightarrow \infty$ . The rescaled system for  $c$  and  $\hat{\phi}$  satisfies Eqs. (1) & (2), but with a rescaled Péclet number  $\text{Pe}(t) = \text{Pe}a(t)$ . In addition, the normal growth in the  $w$  plane is  $\sigma_w = \sigma/|g'|$  to take into account the local volumetric scaling of the conformal map.

Even in the  $w$  plane where the object is the unit circle, the concentration  $c$  cannot be determined analytically. However, asymptotic expansions have been studied in detail [41], and for Péclet numbers below 0.1, the approximation

$$\sigma_w \sim \frac{\lambda I_0(\tilde{\text{Pe}})e^{\tilde{\text{Pe}} \cos \theta}}{K_0\left(\frac{\tilde{\text{Pe}}}{2}\right)} - \lambda \tilde{\text{Pe}} \left( \cos \theta + \int_0^{\tilde{\text{Pe}}} \frac{I_1(t)e^{t \cos \theta}}{t} dt \right), \quad (5)$$

is uniformly accurate in  $\theta = \arg w$ . Taking the leading term of this approximation gives

$$\sigma_w \sim \frac{\lambda(1 + \tilde{\text{Pe}} \cos \theta)}{-\gamma - \log \frac{\tilde{\text{Pe}}}{4}} - \lambda \tilde{\text{Pe}} \cos \theta, \quad (6)$$

where  $\gamma$  is Euler’s constant.

To make progress, we now focus on the intermediate regime starting at small Péclet number and ending prior to collapse, in which it is reasonable to assume that  $\log \text{Pe}$  is a constant [44]. By rescaling the time, we choose  $\lambda = \gamma + \log \frac{\text{Pe}}{4}$  without loss

of generality. If the constant  $B = \text{Pe}\lambda$  is introduced, which we subsequently refer to as the flow strength, then Eq. (6) becomes

$$\sigma_w = -1 + Ba(t) \cos \theta. \quad (7)$$

To transform this back into the physical domain, consider a point on the  $z(t) = g(w(t), t)$  on the boundary  $S(t)$  of the object. Taking a time derivative gives  $\dot{z} = g' \dot{w} + \dot{g}$ . Multiplying by  $\overline{wg'}$  and taking the real part gives

$$\text{Re}(\overline{wg'} \dot{z}) = \text{Re}(\overline{wg'} g' \dot{w}) + \text{Re}(\overline{wg'} \dot{g}). \quad (8)$$

Since the point in the  $w$  plane mapping to  $z(t)$  must lie on the unit circle, it follows that  $w\bar{w} = 1$  and hence  $\text{Re}(\bar{w}\dot{w}) = 0$ , so the first term on the right hand side of Eq. (8) vanishes. The motion of the point in the  $z$  plane is  $\dot{z} = \sigma \hat{n}$  where  $\hat{n}$  is the normal vector written as a complex number. Taking into account rotation and scaling, the normal vector is given by

$$\hat{n} = \frac{g'}{|g'|} \frac{w}{|w|} \quad (9)$$

and hence the left hand side of Eq. (8) is

$$\text{Re}(\overline{wg'} \dot{z}) = \text{Re} \left( \frac{\overline{wg'} g' w \sigma}{|g' w|} \right) = \text{Re}(|g'| \sigma) = \sigma_w. \quad (10)$$

Combining Eqs. (7), (8), and (10) yields

$$\text{Re}(\overline{wg'} \dot{g}) = -1 + Ba(t) \cos \theta, \quad (11)$$

which describes the dissolution process in terms of a time-dependent conformal map. For  $B = 0$  it becomes the Polubarinova–Galin equation [26–28], which has been used in previous continuum DLA (viscous fingering) studies without advection [23, 29]. The incorporation of the  $Ba(t) \cos \theta$  term [44] represents the simplest extension to account for the general effect of advection [38] and is therefore a useful and interesting model to study in its own right.

### III. NUMERICAL METHOD AND IMPLEMENTATION

#### A. Discrete formulation of the governing equation

We now make use of Eq. (11) to formulate a numerical solution technique. We represent the dissolving object via the time-dependent conformal map in Eq. (4) with a fixed value of  $N \geq 1$ . We write the  $q_n(t)$  in component form as  $b_n(t) + ic_n(t)$ , and describe the shape of the object by the real vector  $\mathbf{s}(t) = (a, b_0, b_1, \dots, b_N, c_0, c_1, \dots, c_N)$ , with a total of  $2N + 3$  components. Using the two expressions

$$\overline{wg'} = a\bar{w} - \sum_{n=0}^N n(b_n - ic_n)\bar{w}^{-n}, \quad (12)$$

$$\dot{g} = \dot{a} + \sum_{n=0}^N (\dot{b}_n + i\dot{c}_n)w^{-n}, \quad (13)$$

Eq. (11) becomes

$$-1 + Ba \cos \theta = \text{Re} \left( \left[ ae^{-i\theta} - \sum_{n=0}^N n(b_n - ic_n)e^{in\theta} \right] \left[ \dot{a}e^{i\theta} + \sum_{n=0}^N (\dot{b}_n + i\dot{c}_n)e^{-in\theta} \right] \right). \quad (14)$$

Eq. (14) is real, and can be expressed in terms of components  $\cos n\theta$  and  $\sin n\theta$  for  $n = 1, \dots, N + 1$ , plus a constant term. Equating both sides of the Eq. (14) in each component leads to  $2N + 3$  coupled ordinary differential equations for the  $2N + 3$  variables  $a(t)$ ,  $b_n(t)$ , and  $c_n(t)$ . Hence, other than for cases where these equations are degenerate,  $\mathbf{s}$  will be uniquely determined in terms of  $\mathbf{s}$ . Furthermore, since Eq. (14) does not feature any higher harmonic of sine and cosine, it follows that  $\mathbf{s}$  exactly represents the time-evolution prescribed by Eq. (11): if a shape initially is described in terms of a Laurent series using terms up to  $q_N$ , it will remain perfectly described by this Laurent series throughout the whole dissolution process.

The details of equating each component of Eq. (14) are given in Appendix A. Equating the constant terms gives

$$a\dot{a} - \sum_{n=0}^N n(b_n\dot{b}_n + c_n\dot{c}_n) = -1. \quad (15)$$

Equating the terms with factors  $\cos(N + 1)\theta$  and  $\sin(N + 1)\theta$  gives

$$a\dot{b}_N = \dot{a}Nb_N, \quad a\dot{c}_N = \dot{a}Nc_N, \quad (16)$$

respectively. Equating the terms with a factor of  $\sin n\theta$  for  $n = 1, \dots, N$  gives

$$0 = -\dot{a}(n - 1)c_{n-1} + a\dot{c}_{n-1} - \sum_{m=0}^{N-n} \left[ (m + n)(c_{m+n}\dot{b}_m - b_{m+n}\dot{c}_m) - m(c_m\dot{b}_{m+n} - b_m\dot{c}_{m+n}) \right] \quad (17)$$

Finally, equating the terms with a factor of  $\cos n\theta$  for  $n = 1, \dots, N$  gives

$$\beta_n = -\dot{a}(n - 1)b_{n-1} + a\dot{b}_{n-1} - \sum_{m=0}^{N-n} \left[ (m + n)(b_{m+n}\dot{b}_m + c_{m+n}\dot{c}_m) + m(b_m\dot{b}_{m+n} + c_m\dot{c}_{m+n}) \right] \quad (18)$$

where  $\beta_n = Ba$  if  $n = 1$ , and  $\beta_n = 0$  otherwise. The combination of Eqs. (15), (16), (17), and (18) can then be expressed as a linear system

$$M(\mathbf{s})\dot{\mathbf{s}} = \mathbf{v}(\mathbf{s}) \quad (19)$$

where  $M$  and  $\mathbf{v}$  are matrix and vector functions of  $\mathbf{s}$ , respectively. By writing Eq. (19) as  $\dot{\mathbf{s}} = M^{-1}(\mathbf{s})\mathbf{v}(\mathbf{s})$ , the system can be integrated numerically.



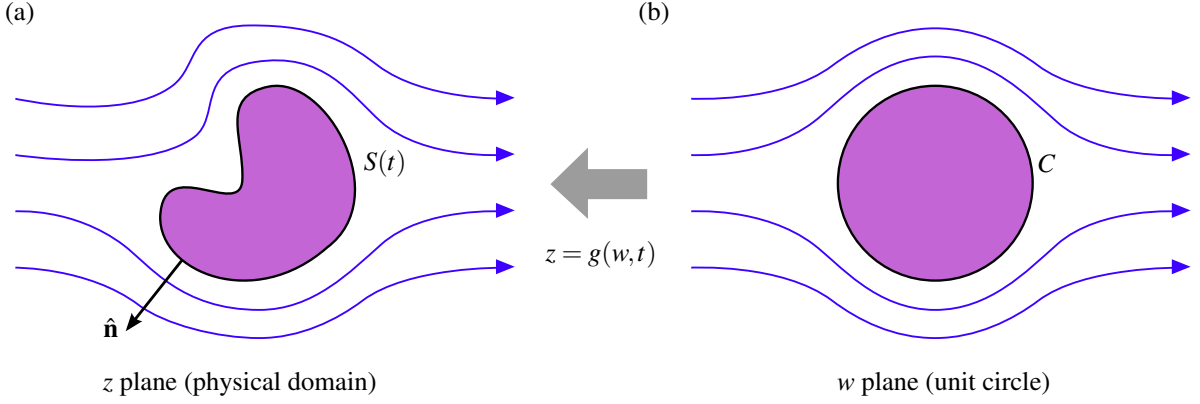


FIG. 1. (a) The physical problem considered, where a two-dimensional object with time-dependent boundary  $S(t)$  is dissolved a chemical concentration being transported by an incompressible potential flow. (b) A reference domain of the same physical problem but where the boundary is the unit circle  $C$ . A time-dependent conformal map  $z = g(w, t)$  describes the transformation between the two domains.

## B. Numerical implementation

The simulations are carried out using double-precision floating point arithmetic, using LAPACK [58] to invert the linear system in Eq. (19). To time-integrate the equation, the DOP853 integration routine described by Hairer *et al.* [56] is used. This routine uses the eighth-order, thirteen-step Dormand–Prince integration method that has the first-same-as-last (FSAL) property, requiring twelve function evaluations per timestep [59]. As described in more detail later, the components of  $s$  can sometimes vary rapidly, particularly close to the time of collapse. The DOP853 routine employs adaptive timestepping, which can retain accuracy in this situation. The routine estimates the local error [60] using a combination of fifth-order and third-order embedded numerical schemes. For all of the subsequent results, the timestep size  $\Delta t$  is continually adjusted so that the absolute local error per timestep remains below a tolerance of  $10^{-14}$ . If the estimated error of a timestep exceeds the tolerance, then the timestep is rejected and the integrator tries again with a reduced  $\Delta t$ .

There are three scenarios where the DOP853 integrator terminates early: (i) if a maximum number of timesteps is reached, (ii) if the equations are detected as stiff [57], or (iii) if the timestep  $\Delta t$  required achieve the desired local error becomes too small. In the following results, we have only observed the third scenario. This occurs when  $\Delta t$  becomes smaller than  $10u_r t$ , where  $u_r = 2.3 \times 10^{-16}$  is an estimate of the smallest number satisfying  $1.0 + u_r > 1.0$  in double-precision floating point arithmetic. In certain cases, such as the examples of Subsecs. VIA and VIC, the third scenario signifies a breakdown of the physical problem due to the formation of a cusp. However, the third scenario also occurs in normal cases close to the time of collapse  $t_c$  due to  $a(t)$  varying rapidly. If the DOP853 integrator terminates within  $10^4 u_r$  of  $t_c$  then we manually advance to  $t_c$  using timesteps of  $10u_r$  or less. While this may no longer achieve the required level of local error, we find that it provides several additional digits of accuracy in the collapse point location, which is useful in some of the later analysis.

In some of the subsequent results, we must evaluate  $s$  at time points spaced at fixed intervals, which may not precisely coin-

cide with the time points that are selected during the adaptive time-integration, which are usually unevenly spaced. To solve this we use the dense output formulae described by Hairer *et al.* [56]. By performing three additional integration steps, the solution can be approximated as a seventh-order polynomial over the interval of a timestep, allowing  $s$  to be evaluated at any specific time point. For computational efficiency, these three additional steps are only done when one or more output time points overlaps with the current timestep interval.

The simulations are implemented in C++, and the code required to perform all of the subsequent analysis is provided as Supplementary Information. For all of the results presented here, the computation time required to simulate the dissolution process is negligible, taking less than 0.25 s on a Mac Pro (Late 2013) with an 8-core 3 GHz Intel Xeon E5 processor.

## IV. RESULTS

### A. Analytic results for the area and highest mode amplitude

Before presenting results of the numerical method, it is useful to establish some basic features of the equations presented in the previous section. The area of the object is given by

$$A(t) = \iint_{\Omega} dz \quad (20)$$

where  $\Omega$  is the region enclosed by  $S(t)$ . Using Green's identity in complex form,

$$A(t) = -\frac{1}{2i} \oint_{S(t)} z d\bar{z} = \frac{1}{2i} \int_C g(w) \overline{g'(w)} dw. \quad (21)$$

Since  $w\bar{w} = 1$  on the unit circle, the integrand can be converted into an analytic function,

$$\begin{aligned} A(t) &= \frac{1}{2i} \int_C g(w) \overline{g'(w)} \frac{dw}{w^2} \\ &= \frac{1}{2i} \int_C \left( a - \sum_{n=0}^N q_n n w^{-(n+1)} \right) \left( \frac{a}{w} + \sum_{n=0}^N \bar{q}_n w^n \right) dw \end{aligned} \quad (22)$$

and applying residue calculus gives

$$A(t) = \pi \left( a^2 - \sum_{n=0}^N n |q_n|^2 \right) = \pi \left( a^2 - \sum_{n=0}^N n (b_n^2 + c_n^2) \right), \quad (23)$$

describing the area as a function of the current mode amplitudes. Furthermore, time-integrating Eq. (15) gives

$$a^2 - \sum_{n=0}^N n (b_n^2 + c_n^2) = C - 2t, \quad (24)$$

where  $C$  is a constant, and hence

$$A(t) = A_0 - 2\pi t, \quad (25)$$

where  $A_0$  is the initial area of the object. The area of the object therefore decreases at a constant rate, independent of the flow parameter  $B$ , with the time to collapse given by

$$t_c = \frac{A_0}{2\pi} = \frac{1}{2} \left( a^2 - \sum_{n=0}^N n |q_n|^2 \right). \quad (26)$$

The modes in Eq. (16) also have first integrals,

$$b_N = k a^N, \quad c_N = l a^N \quad (27)$$

for some constants  $k$  and  $l$ . The highest mode amplitudes are therefore only dependent on the conformal radius  $a$ . Due to the couplings in Eqs. (17) and (18), similar results for the lower modes do not exist.

## B. Initial numerical results

Figure 2 shows the dissolution process for six objects calculated using the numerical code, where for all cases  $a(0) = 1$  and  $B = 0.7$ . Figure 2(a) shows the dissolution process for a circle. Throughout the process, the circle retains its shape although its center progressively moves rightward due to the effect of the flow, which preferentially dissolves the side of the circle facing upstream. A similar behavior is visible in Fig. 2(b) for an ellipse, which keeps its shape through the dissolution process, while the ellipse center moves up and right. The results for Figs. 2(a) and 2(b) match those that were previously studied analytically [44]. For the case of no flow where  $B = 0$  where the system is mathematically equivalent to (time-reversed) Laplacian growth, and bubble contraction in a porous medium, it is known that the ellipse is the most generic self-similar shape [61–63].

Figure 2(c) shows the dissolution process for a triangular-shaped object given by setting  $q_2 = -0.35$  initially. In general, the mode  $q_n$  is responsible for an  $(n+1)$ -fold perturbation of the boundary. If all of the  $q_n$  are initially real, the object is symmetric about the  $x$  axis, and will remain symmetric throughout the dissolution process. For the case shown, the point of the triangle that faces upstream is more rapidly dissolved than the other two. Unlike the previous two examples that retain their shape during dissolution, the triangle becomes progressively

more rounded at later times. Figure 2(d) shows the dissolution process when the previous object is rotated by  $90^\circ$ , which is achieved by setting  $q_2 = 0.35i$ . This object is initially symmetric about the  $y$  axis, but the flow causes this symmetry to be lost as time passes. The collapse point is slightly up and right from the origin.

Figure 2(e) shows the dissolution process for the case when  $q_{15} = 0.05i$  initially, which creates a 16-fold perturbation in the boundary. After 20% of the object has dissolved, this perturbation is almost completely removed, with the object's shape approaching that of a circle. This is expected from Eq. (27), which shows that the highest mode will be proportional to  $a^N$  and hence decay more rapidly for larger  $N$ . If several modes are initially non-zero as in Fig. 2(f) an irregular shape is formed, which behaves like a combination of the previous examples, with sharp features in the boundary being rapidly removed.

We now examine the evolution of the modes and look in detail at the effect of the flow strength  $B$ . We make use of the specific example of a diamond shape given by  $a = 1$  and  $q_3 = 0.25$  initially. Figure 3(a) shows the dissolution process for the case of zero flow when  $B = 0$ . Similar to Figs. 2(c) and 2(d) the object becomes progressively more circular, but without the presence of flow it retains symmetry in the  $x$  axis,  $y$  axis, and the line  $x = y$ . Figure 3(b) shows the time-evolution of the modes throughout the dissolution process. The modes  $q_0, q_1, q_2$ , which were zero initially, remain zero throughout the dissolution process—this is expected since any non-zero contribution from these modes would break at least one of the symmetries seen in Fig. 3(a). The dissolution process is therefore described entirely in terms of  $a$  and  $q_3$ , and could therefore be determined analytically using Eqs. (24) and (27), as considered in previous work [29, 44, 64]. Since  $q_0$  remains at zero, the collapse point is at the origin.

Figure 3(c) shows the dissolution of the diamond when the flow parameter is  $B = 0.7$ . As in the previous examples of Fig. 2, the diamond dissolves more rapidly on the side facing upstream, and the collapse point is slightly downstream. The time evolution of the modes (Fig. 3(d)) is significantly altered in this case, with all three components  $q_0, q_1$ , and  $q_2$  becoming non-zero during the dissolution process, due to the mixing between modes via the advection term in Eq. (11). The effects of these three modes, such as the translation of the object center, and the loss of symmetry about the  $y$  axis, are clearly visible in Fig. 3(c). The  $q_1$  and  $q_2$  modes decay to zero at the point of collapse, while the  $q_0$  mode remains positive. The value of  $q_0$  at  $t = t_c$  gives the collapse point position.

Figures 3(b) and 3(d) also indicate the adaptive integration timesteps chosen by the DOP853 integration routine. In the middle of the dissolution process, at  $t \approx 0.2$ , the routine is able to take timesteps up to approximately 0.02 while retaining the desired level of local error of  $10^{-14}$ . However, close to  $t = t_c$ , many more timesteps are needed to resolve the rapid change in  $a$ . For the example shown in Fig. 3(d), a total of 329 integration timesteps are evaluated. During the DOP853 integration routine, 194 steps are accepted, and 128 are rejected due to the local error estimate exceeding the given tolerance. Six additional small steps are required to reach the collapse time  $t_c$ .

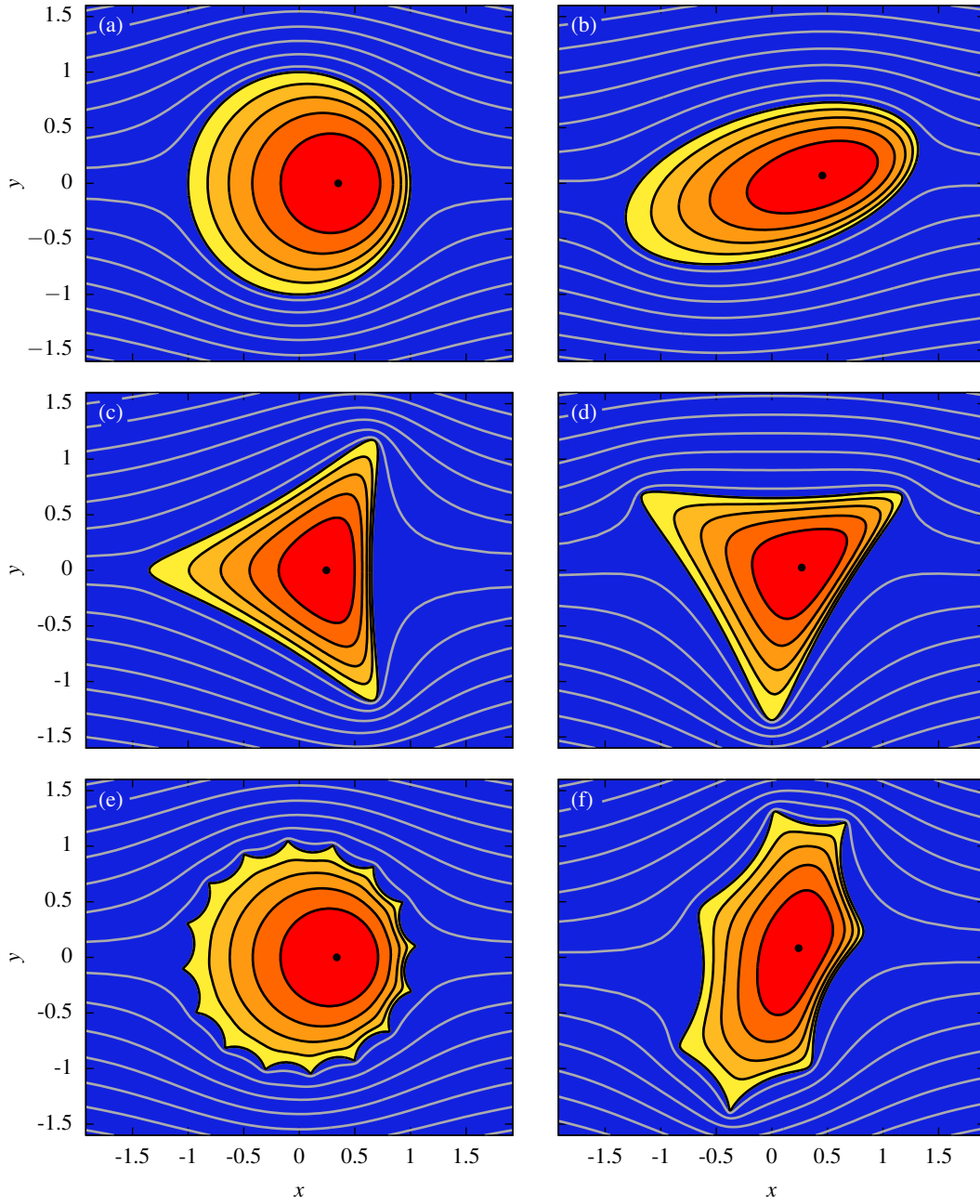


FIG. 2. Sample dissolution processes for six objects, all starting with  $a = 1$  and using  $B = 0.7$ . The six objects and initial non-zero modes are (a) a circle, (b) an ellipse with  $q_1 = 0.3 + 0.2i$ , (c) a triangle with  $q_2 = -0.35$ , (d) a triangle with  $q_2 = 0.35i$ , (e) a corrugated circle with  $q_{15} = 0.05i$ , and (f) an irregular object with  $q_1 = -0.28 + 0.2i$  and  $q_6 = 0.1$ . The white lines show the flow streamlines around the initial shape. The colored regions shown the shapes of the object at successive times as it dissolves, where each progressive region represents the dissolution of 20% of the object's initial area. The black circles indicate the final points of collapse.

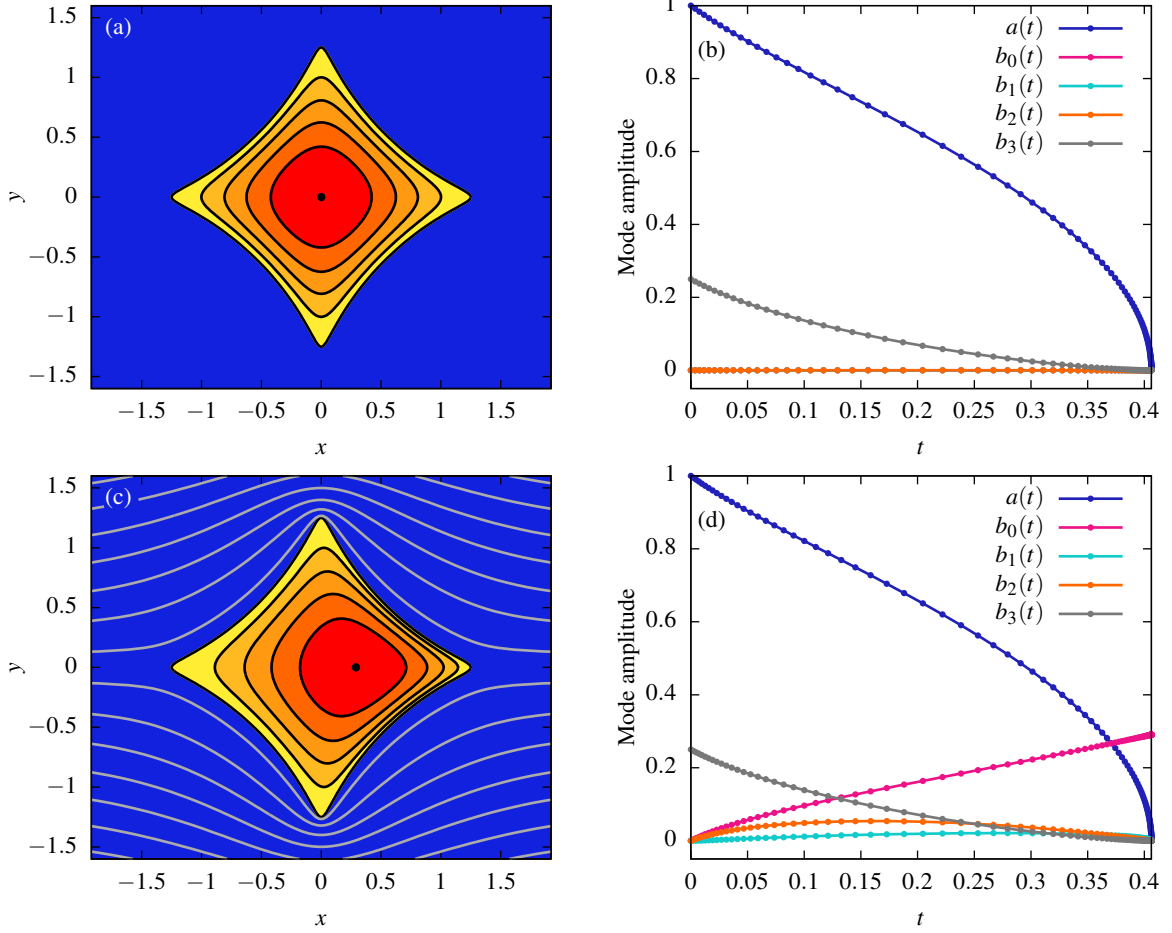


FIG. 3. (a) Dissolution process of a diamond shape initially described by non-zero modes  $a = 1$  and  $q_3 = 0.25$  for the case of zero flow,  $B = 0$ . The colored regions shown the shapes of the object at successive times as it dissolves, where each progressive region represents the dissolution of 20% of the object's area, with the black circle indicating the point of collapse. (b) Time-evolution of the modes describing the diamond during dissolution, where the small circles on each curve show the integration timesteps using the adaptive DOP853 integration scheme. (c) Dissolution process of the diamond when the flow is  $B = 0.7$ . (d) Time-evolution of the modes describing the diamond during dissolution with flow, with the small circles on each curve showing the integration timesteps.

### C. Inferring analytic formulae for the collapse point

Figures 2 and 3 show that the collapse point  $z_c = x_c + iy_c$  of the dissolution process is dependent on both the flow strength  $B$  and the initial shape of the body as described by its Laurent coefficients. Since there are no other quantities in the problem,  $z_c$  must be given in terms of  $B$  and the Laurent coefficients only. The precise form of this dependence is not obvious, as the collapse point is given as the component  $q_0$  of the nonlinear differential equation system, evaluated at the time of collapse  $t_c$ .

In this section, we infer the exact form of this relationship by exploiting the very high accuracy of the simulations, which allow the collapse point to be calculated to at least twelve decimal places. To simplify the analysis, we set  $a = 1$  throughout this section. To begin, we restrict to the case when the Laurent coefficients are given purely in terms of real components  $b_j$ . As discussed in the previous section, the components will

remain real throughout the simulation, and the object will be symmetric about the  $x$  axis. Hence the collapse point  $z_c$  will be real, and determined entirely in terms of the horizontal position  $x_c$ .

Figure 4 shows an example of inferring an analytic relationship, for the case of an ellipse where the only non-zero Laurent coefficient is  $b_1$ . Figures 4(a–d) show four dissolution process are shown for when  $b_1 = 0.3$  and the flow strength is  $B = 0, 0.3, 0.6, 0.9$ , respectively. The collapse point  $x_c$  moves progressively right as  $B$  is increased. In Fig. 4(e), the numerically computed  $x_c$  is plotted as a function of  $B$ , for three different values of  $b_1$  of 0.0, 0.3, and 0.6. The plot demonstrates that  $x_c$  is linear in  $B$ , with the slope depending on  $b_1$ . The numerical data matches the relationship

$$x_c = \frac{B(1+b_1)}{2}, \quad (28)$$

with the sum of square residuals being  $1.3 \times 10^{-30}$ ,  $1.3 \times$



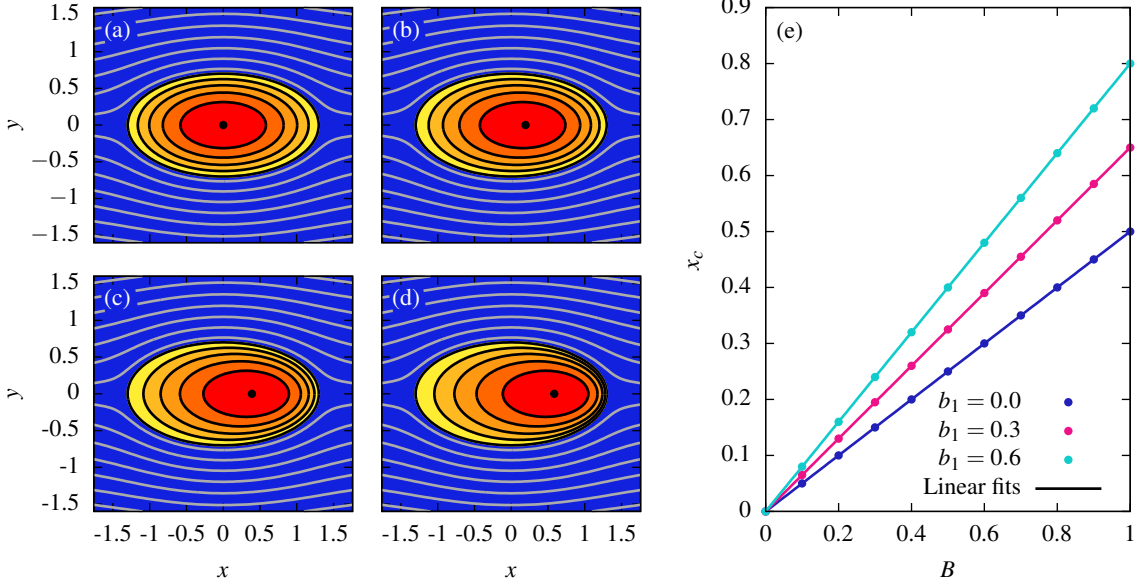


FIG. 4. An example procedure to infer the analytic formula for position of collapse point in terms of the initial modes. (a–d) Dissolution processes of an ellipse given by  $a = 1, q_1 = 0.3$  for flow strengths of  $B = 0, 0.3, 0.6, 0.9$ , respectively, using the same visual representation as described in Fig. 2. (e) Plot of the numerically computed horizontal collapse point position  $x_c = \text{Re} z_c$  as a function of  $B$  for three different values of  $b_1$ , which match linear relationships to numerical precision, suggesting an analytical relationship.

$10^{-30}$ , and  $4.5 \times 10^{-30}$  for  $b_1 = 0, 0.3, 0.6$ , respectively. These small residuals, which are of a similar size to the expected numerical error, strongly suggest that this is an exact relationship for the original mathematical problem.

One can extend this analysis to the case where the only non-zero Laurent coefficient is  $b_n$ , and determine that  $x_c$  satisfies the polynomial relationship

$$\frac{B}{2} = \frac{x_c - b_n x_c^n}{1 - n b_n^2 x_c^{n-1}}. \quad (29)$$

For  $n = 1$ , this is consistent with Eq. (28) for the ellipse, although it also reveals more structure, and by substituting Eq. (26) the relationship simplifies to

$$B t_c = x_c - b_n x_c^n. \quad (30)$$

To proceed, we now consider if there are two non-zero Laurent coefficients. The simplest case would be  $b_0$  and  $b_n$  being non-zero, for  $n \geq 1$ . Since  $b_0$  corresponds to a translation, the relationship is immediately given by

$$B t_c = (x_c - b_0) - b_n (x_c - b_0)^n, \quad (31)$$

without the need for simulation. Expanding the second term yields

$$B t_c = -b_n x_c^n + n b_n b_0 x_c^{n-1} - \frac{n(n-1)}{2} b_n b_0^2 x_c^{n-2} + \frac{n(n-1)(n-2)}{6} b_n b_0^3 x_c^{n-3} - \dots + (x_c - b_0) \quad (32)$$

where the coefficients on the powers of  $x_c$  follow Pascal's triangle.

The next case to consider is when  $b_1$  and  $b_n$  are non-zero, for  $n \geq 2$ . Unlike the previous case this cannot be immediately derived, and must be inferred through fitting to simulation. Table I shows the derived results for the cases of  $n = 2, 3, \dots, 10$  where a surprising pattern emerges. We see polynomials that bear some resemblance to a binomial expansion, although in contrast to Eq. (32), only every second power of  $x_c$  is present. Furthermore, the coefficients in front of the terms are integer, but of a more complicated form than Pascal's triangle. Unlike the previous case, the more complicated form of these polynomials precludes rewriting them in a succinct form like Eq. (31). The pattern continues for the case when  $b_2$  and  $b_n$  are non-zero, for  $n \geq 3$ . As shown in Table II, only every third power of  $x_c$  is present. The integer coefficients follow a natural progression from those in Table I.

In Tables I and II, we observe that each pair of non-zero Laurent coefficients leads to a combination of additional terms appearing in the collapse point polynomial. Building on these results, we inferred and numerically tested the formula

$$B t_c = -b_4 x_c^4 - x_c^3 + x_c^2 (4b_4 b_1 - b_2) + x_c (1 - b_1 + 3b_3 b_1 + 4b_4 b_2) + 2b_2 b_1 + 3b_3 b_2 + 4b_4 b_3 - 2b_4 b_1^2 \quad (33)$$

for the case of all four coefficients  $b_1, b_2, b_3$ , and  $b_4$  being non-zero. In Eq. (33) all terms involve powers of two different  $b_n$ , but for higher non-zero Laurent coefficients, terms with three or more different  $b_n$  arise. If  $b_1, b_2$ , and  $b_5$  are non-zero, then we find that

$$B t_c = -b_5 x_c^5 + 5b_5 b_1 x_c^3 + (5b_5 b_2 - b_2) x_c^2 + (1 - b_1 - 5b_5 b_1^2) + 2b_2 b_1 - 4b_5 b_2 b_1, \quad (34)$$

$n$	$Q(x_c)$
2	$-b_2x_c^2 + 2b_2b_1 + (1-b_1)x_c$
3	$-b_3x_c^3 + 3b_3b_1x_c + (1-b_1)x_c$
4	$-b_4x_c^4 + 4b_4b_1x_c^2 - 2b_4b_1^2 + (1-b_1)x_c$
5	$-b_5x_c^5 + 5b_5b_1x_c^3 - 5b_5b_1^2x_c + (1-b_1)x_c$
6	$-b_6x_c^6 + 6b_6b_1x_c^4 - 9b_6b_1^2x_c^2 + 2b_6b_1^3 + (1-b_1)x_c$
7	$-b_7x_c^7 + 7b_7b_1x_c^5 - 14b_7b_1^2x_c^3 + 7b_7b_1^3x_c + (1-b_1)x_c$
8	$-b_8x_c^8 + 8b_8b_1x_c^6 - 20b_8b_1^2x_c^4 + 16b_8b_1^3x_c^2 - 2b_8b_1^4 + (1-b_1)x_c$
9	$-b_9x_c^9 + 9b_9b_1x_c^7 - 27b_9b_1^2x_c^5 + 30b_9b_1^3x_c^3 + 9b_9b_1^4x_c + (1-b_1)x_c$
10	$-b_{10}x_c^{10} + 10b_{10}b_1x_c^8 - 35b_{10}b_1^2x_c^6 + 50b_{10}b_1^3x_c^4 - 25b_{10}b_1^4x_c^2 + 2b_{10}b_1^5 + (1-b_1)x_c$
	$-b_nx_c^n + nb_nb_1x_c^{n-2} - \frac{n(n-3)}{2}b_nb_1^2x_c^{n-4} + \frac{n(n-4)(n-5)}{6}b_nb_1^3x_c^{n-6} - \dots + (1-b_1)x_c$

TABLE I. Examples of the analytic relationship  $Bt_c = Q(x_c)$  for the horizontal collapse point position  $x_c$  that were inferred numerically using the high-precision calculations, for the case of an object described by two real non-zero Laurent coefficients  $b_1$  and  $b_n$ . The integer coefficients colored in blue, green, and red follow patterns. The final line of the table shows an inferred general formula.

$n$	$Q(x_c)$
3	$-b_3x_c^3 + 3b_3b_2 + (x_c - b_2x_c^2)$
4	$-b_4x_c^4 + 4b_4b_2x_c + (x_c - b_2x_c^2)$
5	$-b_5x_c^5 + 5b_5b_2x_c^2 + (x_c - b_2x_c^2)$
6	$-b_6x_c^6 + 6b_6b_2x_c^3 - 3b_6b_2^2 + (x_c - b_2x_c^2)$
7	$-b_7x_c^7 + 7b_7b_2x_c^4 - 7b_7b_2^2x_c + (x_c - b_2x_c^2)$
8	$-b_8x_c^8 + 8b_8b_2x_c^5 - 12b_8b_2^2x_c^2 + (x_c - b_2x_c^2)$
9	$-b_9x_c^9 + 9b_9b_2x_c^6 - 18b_9b_2^2x_c^3 + 3b_9b_1^3 + (x_c - b_2x_c^2)$
10	$-b_{10}x_c^{10} + 10b_{10}b_2x_c^7 - 25b_{10}b_2^2x_c^4 + 10b_{10}b_2^3x_c + (x_c - b_2x_c^2)$
11	$-b_{11}x_c^{11} + 11b_{11}b_2x_c^8 - 33b_{11}b_2^2x_c^5 + 22b_{11}b_2^3x_c^2 + (x_c - b_2x_c^2)$
12	$-b_{12}x_c^{12} + 12b_{12}b_2x_c^9 - 42b_{12}b_2^2x_c^6 + 40b_{12}b_2^3x_c^3 - 3b_{12}b_2^4 + (x_c - b_2x_c^2)$
	$-b_nx_c^n + nb_nb_2x_c^{n-3} - \frac{n(n-5)}{2}b_nb_2^2x_c^{n-6} + \frac{n(n-7)(n-8)}{6}b_nb_2^3x_c^{n-9} - \dots + (x_c - b_2x_c^2)$

TABLE II. Examples of the analytic relationship  $Bt_c = Q(x_c)$  for the horizontal collapse point position  $x_c$  that were inferred numerically using the high-precision calculations, for the case of an object described by two real non-zero Laurent coefficients  $b_2$  and  $b_n$ . The integer coefficients colored in blue, green, and red follow patterns. The final line of the table shows an inferred general formula.

where the last term on the right hand side is a product of all three non-zero Laurent coefficients.

The final generalization that we consider is when the Laurent coefficients are complex. The fitting procedure described in Fig. 4 becomes more complicated in this case, since both the horizontal position  $x_c$  and the vertical position  $y_c$  of the collapse point will vary. For the case of the Laurent coefficients  $q_1$  and  $q_4$  being non-zero and complex, we inferred the formula

$$Bt_c = \bar{z}_c - \bar{q}_1z_c - \bar{q}_4z_c^4 + 4\bar{q}_4q_1z_c^2 - 2\bar{q}_4q_1^2, \quad (35)$$

which is a generalization of the formula for  $n = 4$  in Table I. The generalization to complex coefficients introduces conjugates on some terms, and the right hand side is not an analytic function of  $z_c$  due to the first term featuring  $\bar{z}_c$ . If  $q_4 = 0$  also, then Eq. (35) simplifies to

$$\frac{B}{2} = \frac{\bar{z}_c - \bar{q}_1z_c}{1 - q_1\bar{q}_1}, \quad (36)$$

which is equivalent to the formula for an ellipse  $z_c = \frac{B}{2}(1 + q_1)$  that was derived in previous work [44].

## V. DERIVATION OF THE COLLAPSE POINT FORMULAE

The previous section revealed a surprising and complicated connection between the collapse point, initial shape of the object, and the flow strength. Using these numerical results as a guide, we now analytically derive this connection. While the formulae in Tables I and II are complicated, it is reasonable to imagine that the specific coefficients could occur as the residue from a contour integral, perhaps involving the product of several Laurent series, and thus our first step is to consider a general integral quantity and determine its behavior during the dissolution process.

### A. Time-evolution of an integral quantity

Consider the expression

$$I(t) = \oint_{S(t)} F(z) d\bar{z} \quad (37)$$

where  $z = g(w)$ ,  $S(t)$  is the shape of the object, and  $F$  is an arbitrary analytic function. This can be written as

$$I(t) = \oint_C F(g(w)) \overline{g'(w)} d\bar{w}, \quad (38)$$

where  $C$  is the unit circle, and  $w = e^{i\theta}$ . Since  $\bar{w}w = 1$  on the unit circle, this can be converted into the integral of an analytic function,

$$I(t) = - \oint_C F(g(w)) \bar{g}'\left(\frac{1}{w}\right) \frac{dw}{w^2}, \quad (39)$$

which can be written as

$$I(t) = \oint_C F(g(w)) \frac{d}{dw} \left( \bar{g}\left(\frac{1}{w}\right) \right) dw \quad (40)$$

and hence integration by parts can be used to obtain

$$I(t) = - \oint_C F'(g(w)) g'(w) \bar{g}\left(\frac{1}{w}\right) dw. \quad (41)$$

This is the first of two expressions that will be used later. To obtain a second integral expression, consider taking the time derivative, which gives

$$\begin{aligned} \frac{dI}{dt} &= - \oint_C \frac{d}{dw} \left( F'(g(w)) \right) \dot{g}(w) \bar{g}\left(\frac{1}{w}\right) dw \\ &\quad - \oint_C F'(g(w)) \left( \dot{g}'(w) \bar{g}\left(\frac{1}{w}\right) + g'(w) \dot{\bar{g}}\left(\frac{1}{w}\right) \right) dw. \end{aligned} \quad (42)$$

Applying integration by parts to the first integral, transfers the derivative onto the  $\dot{g}(w) \bar{g}(1/w)$  terms. Note that

$$\frac{d}{dw} \left( \dot{g}(w) \bar{g}\left(\frac{1}{w}\right) \right) = \dot{g}'(w) \bar{g}\left(\frac{1}{w}\right) - \frac{\dot{g}(w)}{w^2} \bar{g}'\left(\frac{1}{w}\right) \quad (43)$$

and since the first term of this expression will cancel with one of the terms in second integral of Eq. (42), it follows that

$$\frac{dI}{dt} = - \oint_C F'(g(w)) \left( \frac{\dot{g}(w)}{w^2} \bar{g}'\left(\frac{1}{w}\right) + g'(w) \dot{\bar{g}}\left(\frac{1}{w}\right) \right) dw. \quad (44)$$

By substituting  $w = e^{i\theta}$  and making use of Eq. (11),

$$\begin{aligned} \frac{dI}{dt} &= - \int_0^{2\pi} F'(g(e^{i\theta})) i \left( \dot{g}(e^{i\theta}) \overline{g'(e^{i\theta})} e^{-i\theta} \right. \\ &\quad \left. + g'(e^{i\theta}) \overline{\dot{g}(e^{i\theta})} e^{i\theta} \right) d\theta \\ &= -2i \int_0^{2\pi} F'(g(e^{i\theta})) \operatorname{Re} \left( \overline{g'(e^{i\theta})} e^{i\theta} \dot{g}(e^{i\theta}) \right) d\theta \\ &= 2i \int_0^{2\pi} F'(g(e^{i\theta})) (1 - Ba \cos \theta) d\theta. \end{aligned} \quad (45)$$

This can be written as a contour integral as

$$\begin{aligned} \frac{dI}{dt} &= i \int_0^{2\pi} F'(g(e^{i\theta})) (2 - Ba e^{i\theta} - Ba e^{-i\theta}) d\theta \\ &= \oint_C \frac{F'(g(w)) (2w - Ba - Baw^2) dw}{w^2}, \end{aligned} \quad (46)$$

yielding the second integral expression that will be used later. As a check, it is useful to consider when  $F'(z) = 1$ , in which case the integral matches the one in Eq. (21) for the area of the object. Then

$$\frac{dI}{dt} = \oint_C \frac{(2w - Ba - Baw^2) dw}{w^2} = 2\pi i (2) = 4\pi i \quad (47)$$

and

$$\begin{aligned} I(t) &= - \oint_C \left( a - \sum_{n=0}^N q_n n w^{-(n+1)} \right) \left( \frac{a}{w} + \sum_{n=0}^N \bar{q}_n w^n \right) dw \\ &= -2\pi i \left( a^2 - \sum_{n=0}^N n |q_n|^2 \right) = -2\pi i A(t) \end{aligned} \quad (48)$$

This gives  $\dot{A}(t) = -2$ , which agrees with Eq. (24).

### B. A specific integral quantity

A interesting candidate for the function  $F'$  is

$$F'(z) = \frac{1}{z - z_c} \quad (49)$$

where  $z_c$  is the collapse point. This function is particularly special, since as the object is dissolving, the integrals given in Eqs. (41) and (46) will always be finite, as the integration contour will never pass over the singularity. Even though the function  $F(z) = \log(z - z_c)$  is multivalued, the two integral expressions that will be used in the following derivation, Eqs. (41) and (46), are related to each other through a derivation only involving  $F'$ , and thus it is not necessary to consider branch cuts that would be needed to integrate  $F$ . Equation (46) will give

$$\begin{aligned} \frac{dI}{dt} &= \oint_C \frac{(2w - Ba - Baw^2) dw}{w^2 (aw - z_c + \sum_{n=0}^N q_n w^{-n})} \\ &= \oint_C \frac{(2w - Ba - Baw^2) dw}{aw^3 \left( 1 - \frac{1}{aw} (z_c - \sum_{n=0}^N q_n w^{-n}) \right)}. \end{aligned} \quad (50)$$

Since  $g(w, t)$  is a conformal map that takes the region  $|w| \geq 1$  to the region outside the object, there can be no solutions to  $g(w, t) = z_c$  for  $|w| \geq 1$  and thus the above integrand will have no poles for  $|w| \geq 1$ . Hence the integration contour can be deformed outwards and evaluated in terms of the residue at infinity, which is given by the coefficient of the  $w^{-1}$  term, namely  $-Ba/a = -B$ . Hence

$$\frac{dI}{dt} = -2\pi i B \quad (51)$$

and therefore  $I(t) = D - 2\pi i B t$  for some constant  $D$ . To determine the constant, we consider the limit as  $t \rightarrow t_c$ , where  $a \rightarrow 0$ ,  $q_0 \rightarrow z_c$ , and  $q_n \rightarrow 0$  for all  $n > 0$ . Then Eq. (41) shows that

$$I(t) \rightarrow - \oint_C \frac{a \left( \frac{a}{w} + \bar{q}_0 \right) dw}{(aw - z_c + q_0)} = - \oint_C \frac{a \bar{q}_0}{aw} dw = -2\pi i \bar{z}_c \quad (52)$$

and therefore  $I(t) = 2\pi i (B(t_c - t) - \bar{z}_c)$ . Returning to Eq. (41), and examining the integral at the initial time,

$$I(0) = - \oint_C \frac{\left( a - \sum_{n=0}^N q_n n w^{-(n+1)} \right) \left( \frac{a}{w} + \sum_{n=0}^N \bar{q}_n w^n \right) dw}{aw - z_c + \sum_{n=0}^N q_n w^{-n}}, \quad (53)$$

which for large  $w$  can be expanded as

$$\begin{aligned} I(0) &= - \oint_C \frac{\left( a - \sum_{n=0}^N q_n n w^{-(n+1)} \right) \left( \frac{a}{w} + \sum_{n=0}^N \bar{q}_n w^n \right) dw}{(aw - z_c + \sum_{n=0}^N q_n w^{-n})} \\ &= - \oint_C \frac{\left( a - \sum_{n=0}^N q_n n w^{-(n+1)} \right) \left( \frac{a}{w} + \sum_{n=0}^N \bar{q}_n w^n \right) dw}{aw \left( 1 - \frac{1}{aw} (z_c - \sum_{n=0}^N q_n w^{-n}) \right)} \\ &= - \oint_C \frac{1}{aw} \left( a - \sum_{n=0}^N \frac{n q_n}{w^{n+1}} \right) \left( \frac{a}{w} + \sum_{n=0}^N \bar{q}_n w^n \right) \left( \sum_{k=0}^{\infty} \frac{(z_c - \sum_{n=0}^N q_n w^{-n})^k}{a^k w^k} \right) dw. \end{aligned} \quad (54)$$

This integral will give the desired relationship between  $z_c$  and  $B$ . By expanding out the three power series, and looking at terms of the form  $w^{-1}$  that will give a residue at infinity, the integral will simplify to a polynomial in  $z_c$ . For example, consider the case of only  $q_1$  and  $q_4$  being non-zero. In that case, for  $w$  large, and neglecting terms smaller than  $w^{-1}$ ,

$$\begin{aligned} I(0) &= - \oint_C \left( \frac{1}{w} - \frac{q_1}{aw^3} - \frac{4q_4}{aw^6} \right) \left( \frac{a}{w} + \bar{q}_1 w + \bar{q}_4 w^4 \right) \left( \sum_{k=0}^{\infty} \frac{1}{a^k} \left( \frac{z_c}{w} - \frac{q_1}{w^2} - \frac{q_4}{w^5} \right)^k \right) dw \\ &= - \oint_C \left( \bar{q}_4 w^3 + \bar{q}_1 - \frac{\bar{q}_4 q_1 w}{a} + \dots \right) \left( 1 + \frac{1}{a} \left( \frac{z_c}{w} - \frac{q_1}{w^2} - \frac{q_4}{w^5} \right) + \frac{1}{a^2} \left( \frac{z_c}{w} - \frac{q_1}{w^2} - \frac{q_4}{w^5} \right)^2 + \dots \right) dw \\ &= - \oint_C \left( \frac{1}{w} \left( \frac{\bar{q}_4 z_c^4}{a^4} - \frac{3\bar{q}_4 q_1 z_c^2}{a^3} + \frac{\bar{q}_4 q_1^2}{a^2} + \frac{\bar{q}_1 z_c}{a} - \frac{\bar{q}_4 q_1 z_c^2}{a^3} + \frac{\bar{q}_4 q_1^2}{a^2} \right) + \dots \right) dw \\ &= -2\pi i \left( \frac{\bar{q}_4 z_c^4}{a^4} - \frac{4\bar{q}_4 q_1 z_c^2}{a^3} + \frac{2\bar{q}_4 q_1^2}{a^2} + \frac{\bar{q}_1 z_c}{a} \right). \end{aligned} \quad (55)$$

By using  $I(0) = 2\pi i (B t_c - \bar{z}_c)$  it follows that

$$a^4 B t_c = a^4 \bar{z}_c - \bar{q}_4 z_c^4 + 4a \bar{q}_4 q_1 z_c^2 - 2a^2 \bar{q}_4 q_1^2 - a^3 \bar{q}_1 z_c. \quad (56)$$

If  $a = 1$  then

$$B t_c = \bar{z}_c - \bar{q}_4 z_c^4 + 4\bar{q}_4 q_1 z_c^2 - 2\bar{q}_4 q_1^2 - \bar{q}_1 z_c, \quad (57)$$

which agrees with Eq. (35) that was found numerically.

## VI. THREE EXAMPLES OF THE COLLAPSE POINT EQUATION

For a general case, the collapse point  $z_c$  satisfies the equation

$$0 = P(z_c) = \bar{z}_c - B t_c + \frac{1}{2\pi i} \oint_{S(0)} \log(z - z_c) d\bar{z}, \quad (58)$$

defined at points within the object, where the integral in this equation is evaluated as a polynomial in  $z_c$  following the series

expansion procedure described in the previous section. The polynomial can then be analytically extended to give an expression for  $P(z_c)$  at points outside the object also. However, at points outside the object, the analytic extension will not match the value of the integral, since the enclosed residues will be different. Equation (58) is complicated: it is not analytic due to the presence of  $\bar{z}_c$ , and in general it will contain higher powers of  $z_c$ , so it is likely to have multiple solutions. To use this equation as a predictive tool, it is useful to understand the typical structure of  $P$  and know how to select the correct root. We now consider three examples that explore the structure of  $P$  in relation to the object shape.

### A. First example: an irregular pentagonal shape

Consider an example based on Eq. (57), where the function  $P$  can be written as

$$P(z_c) = \bar{z}_c - B t_c - \bar{q}_4 z_c^4 + 4\bar{q}_4 q_1 z_c^2 - 2\bar{q}_4 q_1^2 - \bar{q}_1 z_c, \quad (59)$$



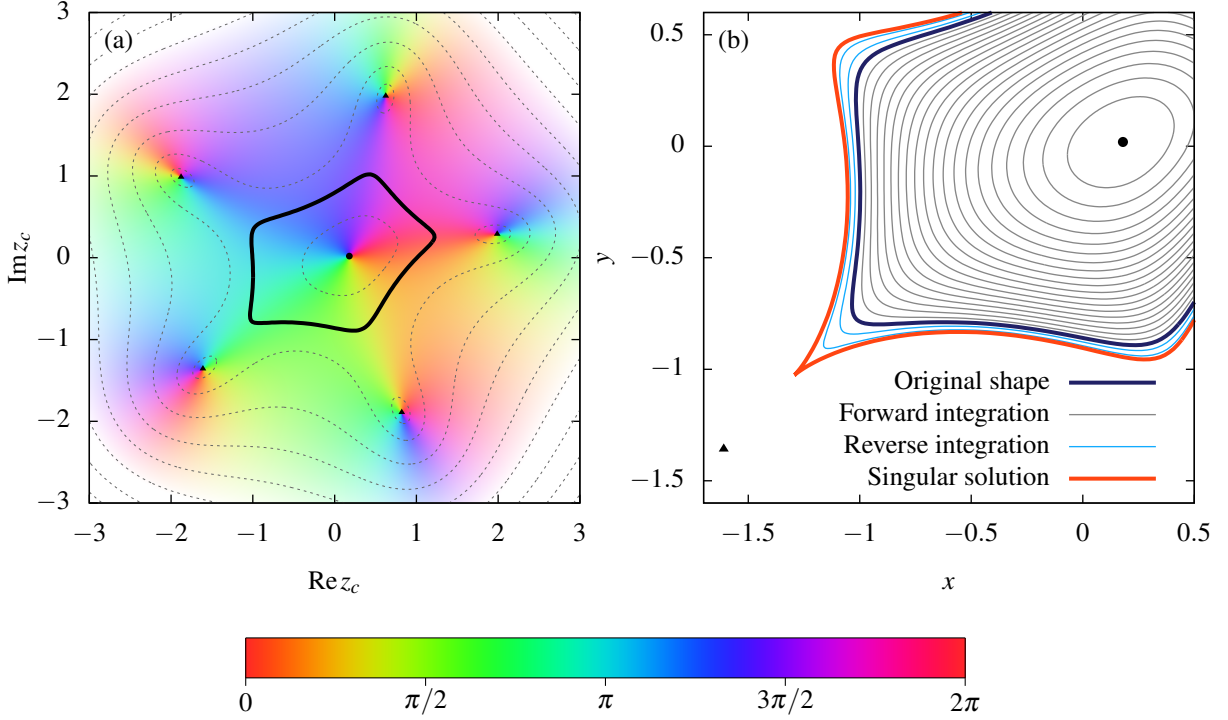


FIG. 5. (a) The thick black line shows an first example object, where  $a = 1$  and the only non-zero Laurent coefficients are  $q_1 = \frac{1}{10} + \frac{3}{20}i$  and  $q_4 = \frac{1}{10} + \frac{1}{20}i$ . The colors show the argument of the function  $P(z)$  for  $B = \frac{7}{20}$ , whose roots represent candidates for the collapse point of the object as it dissolves. The dashed lines are contours of  $|P(z)|$  at the values of  $\frac{n-n+1}{2}$  for  $n \in \mathbb{N}$ . (b) A zoomed-in region showing forward and backward time-evolution of the object boundary at intervals of  $\frac{1}{20}t_c$ . The unique negative-sense root of  $P$  is shown by a circle, and one of the positive-sense roots is shown by a triangle. The four other positive-sense roots are outside the region that is plotted.

where  $t_c = 1 - |q_1|^2 - 4|q_4|^2$ . Fig. 5 shows a plot of the modulus and argument of this function for the case of  $a = 1$ ,  $q_1 = \frac{1}{10} + \frac{3}{20}i$ ,  $q_4 = \frac{1}{10} + \frac{1}{20}i$ , and  $B = \frac{7}{20}$ . The shape of the object is also shown. There are five roots that lie outside the object. There is one root inside the object, which must be the collapse point. Furthermore, the argument in the neighborhood of the interior root rotates in the negative (anti-analytic) sense, whereas the argument near each exterior root rotates in the positive (analytic) sense. By considering the Taylor series of  $P$  at a given root, one can mathematically determine whether a root is positive-sense or negative-sense by whether  $|P_z|^2 - |P_{\bar{z}}|^2$  is positive or negative, respectively. From Eq. (52), the collapse point must be given by a negative-sense root, and hence for this example there is an unambiguous choice, of the single negative-sense root within the object.

It is interesting to consider whether the other roots have physical significance. Figure 5(b) shows a zoomed-in region of the dissolution process for this example, confirming that the interior negative-sense root visible in Fig. 5(a) is indeed the collapse point. The figure also shows a nearby positive-sense root. If the system is time-integrated backward, then the boundary of the object sharpens toward the root. This leads to a cusp singularity in a finite time  $t = -0.06133$ , which appears similar to cusp development in related systems [24, 29, 64]. The cusp formation occurs when a branch point of  $g$  reaches the unit circle. As the cusp is approached, the matrix

$M(s)$  becomes singular, and the DOP853 integrator terminates because the timestep required to keep the local error below the tolerance is smaller than what can be resolved with double precision. While the positive-sense root appears connected to the development of the cusp, it is not located exactly at the cusp, and thus it is not clear what, if any, its precise physical significance is.

A practical way to determine the root positions is to make use of a Newton–Raphson iteration, generalized to take into account that  $P$  also depends on the conjugate of  $z_c$ . An appropriate Newton–Raphson iteration can be constructed by viewing  $P$  as a function of two variables  $z_c$  and  $\bar{z}_c$ , and considering the two-function system of  $P$  and  $\bar{P}$ . For a guess of the form  $z_c^{(n)}$ , the vector generalization of the Newton–Raphson method to give an improved guess  $z_c^{(n+1)}$  is then

$$\begin{pmatrix} P_z & P_{\bar{z}} \\ \bar{P}_z & \bar{P}_{\bar{z}} \end{pmatrix} \begin{pmatrix} z_c^{(n+1)} - z_c^{(n)} \\ \bar{z}_c^{(n+1)} - \bar{z}_c^{(n)} \end{pmatrix} = - \begin{pmatrix} P \\ \bar{P} \end{pmatrix}, \quad (60)$$

which leads to the two equations

$$P_z(z_c^{(n+1)} - z_c^{(n)}) + P_{\bar{z}}(\bar{z}_c^{(n+1)} - \bar{z}_c^{(n)}) = -P, \quad (61)$$

$$\bar{P}_z(z_c^{(n+1)} - z_c^{(n)}) + \bar{P}_{\bar{z}}(\bar{z}_c^{(n+1)} - \bar{z}_c^{(n)}) = -\bar{P}. \quad (62)$$

Substituting Eq. (62) into Eq. (61) to eliminate  $(\bar{z}_c^{(n+1)} - \bar{z}_c^{(n)})$

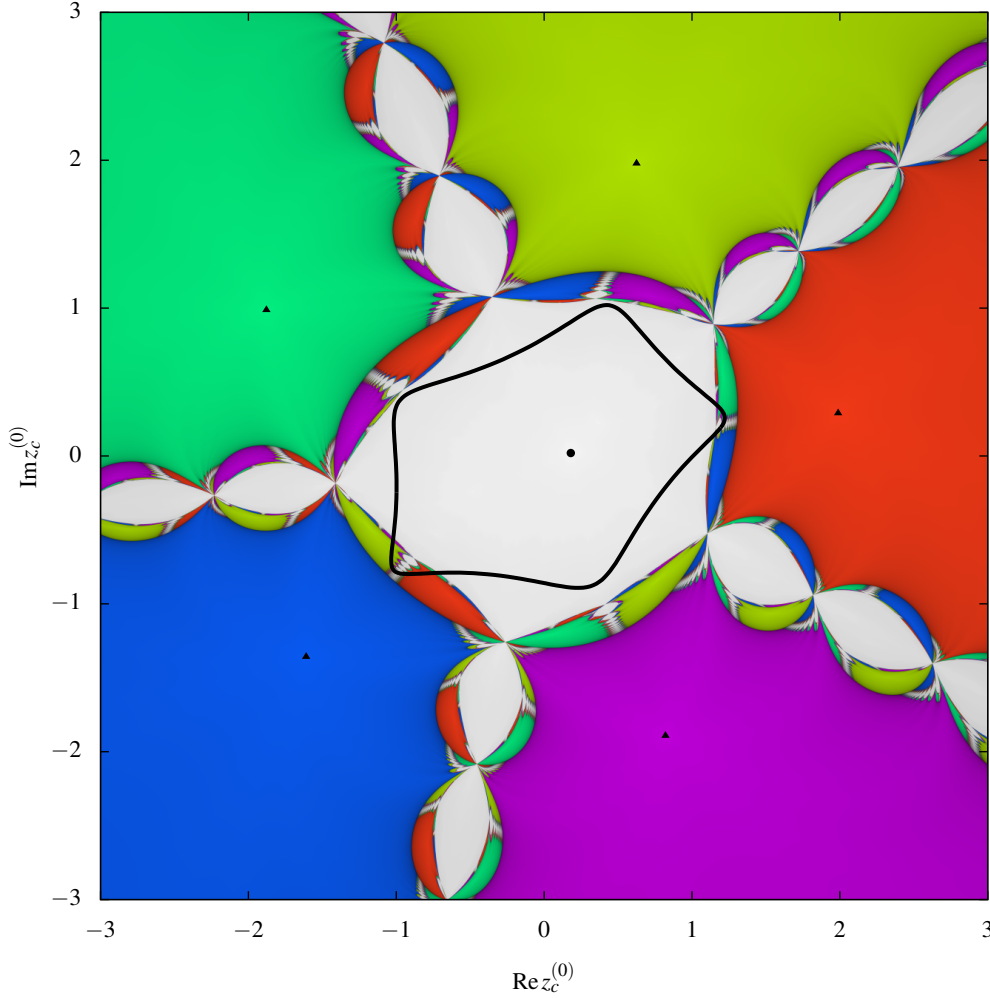


FIG. 6. Plot showing which root of  $P$  a Newton–Raphson iteration will converge to when starting at  $z_c^{(0)}$ , for the example configuration given in Fig. 5. The five positive-sense roots of  $P$  are shown by small black triangles, and the unique negative-sense root is shown by a small black circle. Each point is colored according to the argument of the root that it converges to, with the central root being shown in white. Darker shades show regions that require more iterations to converge.

gives the iterative equation

$$z_c^{(n+1)} = z_c^{(n)} + \frac{\bar{P}P_z - P\bar{P}_z}{|P_z|^2 - |P_{\bar{z}}|^2}. \quad (63)$$

As expected, if  $P_{\bar{z}} = 0$ , then this equation reduces to the standard complex Newton–Raphson iteration.

Figure 6 shows a plot of which root the Newton–Raphson iteration will converge to as a function of the starting guess  $z_c^{(0)}$ . As is typical for Newton–Raphson iterations of complex functions, the plot has a fractal structure, with large basins of attraction surrounding each root. However, the plot has some distinctly different features to usual Newton fractals [65, 66] arising from the vector generalization of the iteration to non-analytic functions. In particular, the denominator  $|P_z|^2 - |P_{\bar{z}}|^2$  featuring in Eq. (63) is zero on a one-dimensional loop of points surrounding the central root. Any starting guess that approaches this loop will therefore undergo a very large initial step. In Fig. 6, this loop forms the dividing line between

the five outer colored basins and the central region. Due to the self-similarity of the fractal, the structure surrounding this loop is replicated in other parts of the plot. This is in noticeable contrast to the regular Newton fractal for an analytic function  $f(z)$ , where the iteration becomes singular only at a zero-dimensional set of points where  $f'(z) = 0$ .

On Figure 6, the object boundary is shown by the dashed black line, and it is almost entirely contained within the central white region, meaning that a starting guess within the object is likely to converge to the collapse point; if the guess is chosen near the center of the object, such as at  $q_0$ , the iteration converges very rapidly and reliably. However the plot also indicates that for several small regions inside the object (e.g. near the bottom left corner) the Newton–Raphson method may converge to one of the exterior roots.

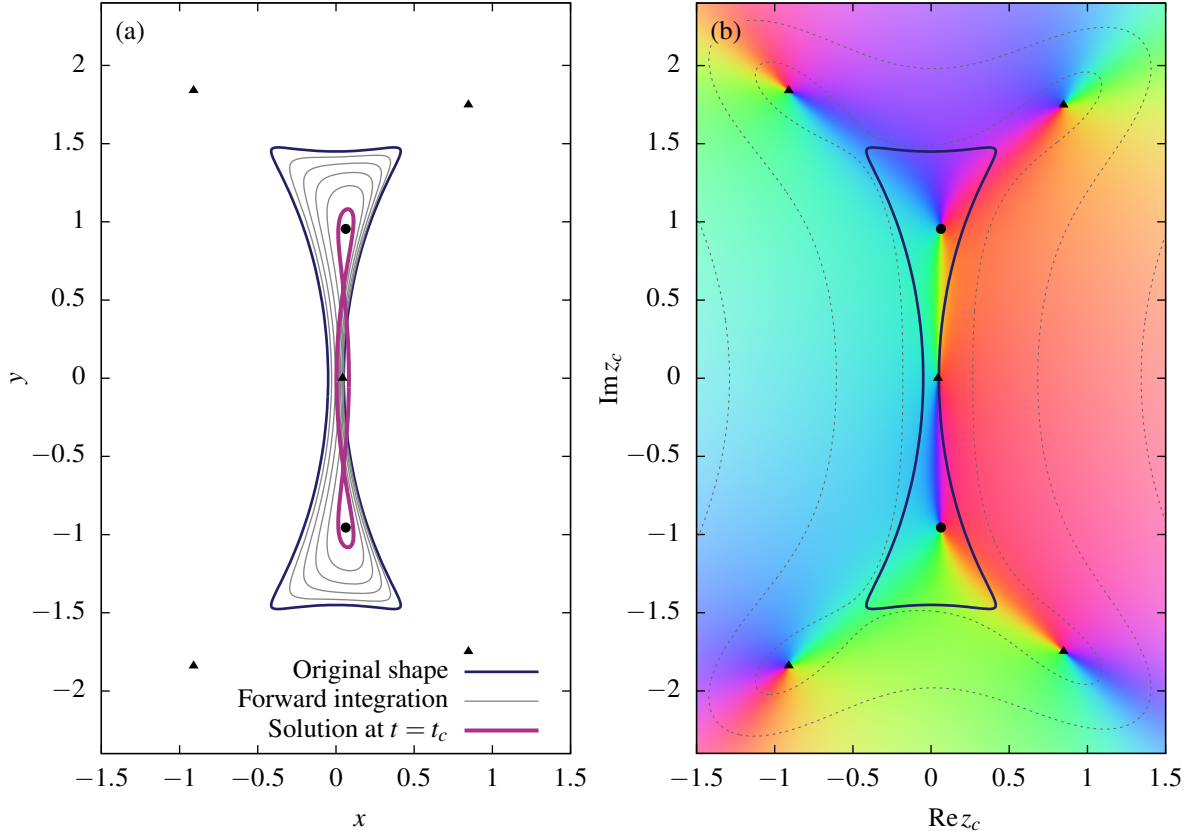


FIG. 7. (a) Time-evolution of a dumbbell-shaped object described by  $a = 1$ ,  $q_1 = -\frac{7}{10}$ ,  $q_3 = -\frac{1}{4}$ ,  $B = \frac{3}{5}$ , and all other Laurent series coefficients are zero. The gray curves are plotted at intervals of  $\frac{1}{5}t_c$ . Positive-sense roots of the function  $P$  are shown by triangles, and negative-sense roots are shown by circles. (b) The structure of the corresponding function  $P$ , with the dashed lines corresponding to contours of  $|P(z)|$  at  $\frac{n-n+1}{4}$  for  $n \in \mathbb{N}$ , and the colors corresponding to the argument using the key given in Fig. 5.

### B. Second example: a dumbbell-shaped object dividing in two

Figure 7(a) shows the dissolution process for the case of a long dumbbell-shaped object, where  $a = 1$ ,  $q_1 = -\frac{7}{10}$ ,  $q_3 = -\frac{1}{4}$ ,  $B = \frac{3}{5}$ , and all other Laurent series coefficients are zero. In this case, the thin vertical sliver dissolves away leaving two separated fragments. While the system can be time-integrated past this point with  $M(s)$  remaining non-singular, the contour begins to overlap with itself, thus losing physical validity. Mathematically, this scenario corresponds to when the function  $g$  from the unit disk to the physical domain becomes multivalued. This is a global property of the function and is therefore a different type of finite-time singularity from the cusp considered in the previous example.

The function  $P$  for this example is

$$P(z_c) = \bar{z}_c - Bt_c - \bar{q}_3 z_c^3 + 3\bar{q}_3 q_1 z_c - \bar{q}_1 z_c,$$

where  $t_c = 1 - |q_1|^2 - 3|q_3|$ . The structure of  $P(z_c)$  and its roots are plotted in Fig. 7(b). The function  $P$  has two negative-sense roots in either end of the dumbbell, four exterior positive-sense roots, and one positive-sense root on the vertical sliver. This example also highlights that the non-analyticity of  $P$  significantly increases its complexity. The last four terms of  $P$  form an analytic cubic function in  $z_c$ , which could have at most

three distinct roots, but adding the anti-analytic  $\bar{z}_c$  increases the number of roots to seven.

While more complicated than the previous example, the positions of the roots appear to be physically reasonable, with one negative-sense root appearing in each end of the dumbbell. The central positive-sense root appears to be associated with the position where the vertical sliver dissolves. However, close inspection reveals that its position is not perfectly aligned with the point where the two sides of the object first come into contact. Instead, it appears to mark the center of the inverted section of the contour at  $t = t_c$ . Figure 8 shows a plot of which root the Newton–Raphson iteration converges to, depending on the starting guess. For starting points  $z_c^{(0)}$  within the object, most will converge to the two negative-sense roots or the central positive-sense root. The denominator  $|P_z|^2 - |P_{\bar{z}}|^2$  in Eq. (63) vanishes on two approximate ellipses surrounding each negative-sense root.

While it is not physically valid to simulate the dissolution of the object to collapse, this example highlights that the structure of  $P$  and the position of its roots may be more complicated than in the previous example considered, and thus any further mathematical analyses would have to take into account this possibility.

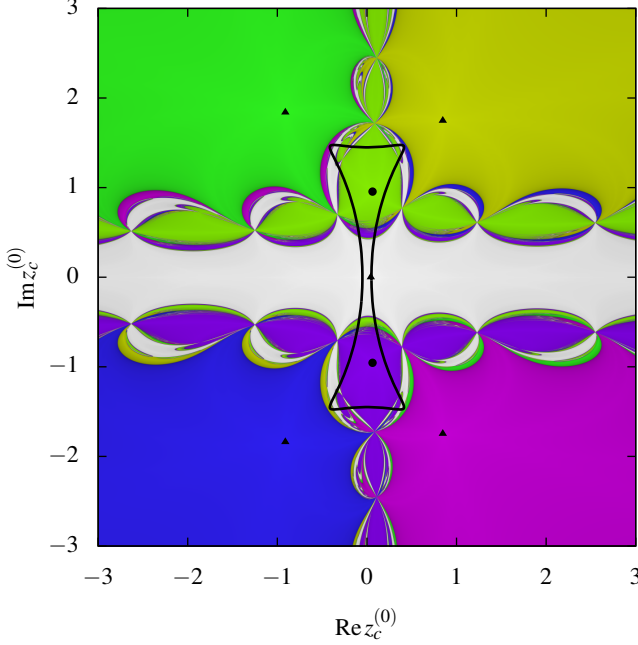


FIG. 8. Plot showing which root of  $P$  a Newton–Raphson iteration will converge to when starting at  $z_c^{(0)}$ , for the dumbbell-shaped example. The five positive-sense roots of  $P$  are shown by black triangles, and the two negative-sense roots are shown by black circles. Each point is colored according to the argument of the root that it converges to, with the central root being shown in white. Darker shades show regions that require more iterations to converge.

### C. Third example: transitions in behavior as flow strength is altered

The final example is a three-pronged object given by the initial non-zero Laurent coefficients  $a = 1$ ,  $q_2 = -\frac{49}{100}$ ,  $q_5 = -\frac{17}{100}$ ,  $q_8 = -\frac{3}{40}$ ,  $q_{11} = -\frac{27}{1000}$ , and  $q_{14} = -\frac{3}{500}$ . Unlike the previous two examples, the collapse point equation is difficult to determine manually due to the large number of Laurent series terms that must be considered. However, a computer code was written that found it to be

$$\begin{aligned}
 P(z_c) = & \bar{z}_c - Bt_c - \bar{q}_{14}z_c^{14} + z_c^{11}(-\bar{q}_{11} + 14\bar{q}_{14}q_2) \\
 & + z_c^8(-\bar{q}_8 + 11\bar{q}_{11}q_2 + 14\bar{q}_{14}q_5 - 63\bar{q}_{14}q_2^2) \\
 & + z_c^5(-\bar{q}_5 + 8\bar{q}_8q_2 + 11\bar{q}_{11}q_5 + 14\bar{q}_{14}q_8 \\
 & - 33\bar{q}_{11}q_2^2 - 84\bar{q}_{14}q_2q_5 + 98\bar{q}_{14}q_2^3) \\
 & + z_c^2(-\bar{q}_2 + 5\bar{q}_5q_2 + 8\bar{q}_8q_5 + 11\bar{q}_{11}q_8 \\
 & + 14\bar{q}_{14}q_{11} - 12\bar{q}_8q_2^2 - 32\bar{q}_{11}q_2q_5 \\
 & - 42\bar{q}_{14}q_2q_8 - 21\bar{q}_{14}q_5^2 + 22\bar{q}_{11}q_2^3 \\
 & + 84\bar{q}_{14}q_2^2q_5 - 35\bar{q}_{14}q_2^4). \quad (64)
 \end{aligned}$$

The left panel of Fig. 9 shows the structure of the solution polynomial when  $B = 0$ . Each of the three prongs is surrounded by five positive-sense roots, and there is a single negative-sense root at the origin. The magnitude of  $P$  within the object is small,

so that most of the object lies within the region  $|P(z_c)| < \frac{1}{4}$ , meaning that an alteration of the flow strength could alter the function’s roots. The right panel shows the function  $P$  when  $B = -\frac{9}{10}$ , corresponding to a strong flow from the right. In this case a new pair of positive-sense and negative-sense roots appear on the real axis, resulting in a similar root arrangement to Fig. 7(b).

Figure 10 shows the dissolution process for three different cases of  $B$ , for a zoomed-in region centered on one of the prongs. The top panel shows the case when  $B = 0$ , where the dissolution process proceeds normally and the object collapses at the single negative-sense root at the origin. Since the physical model given in Eqs. (1), (2), & (3) tends to rapidly dissolve sharply curved boundaries, the three prongs of the object dissolve rapidly enough that they remain connected to each other.

For the case of  $B = \frac{9}{10}$  shown in the bottom panel of Fig. 10 the situation is different. The incorporation of flow into the evolution equation of Eq. (11) causes the thin part of the prong to dissolve more rapidly than its end, meaning that in this case, the object becomes disconnected into two regions. The behavior is similar to the previous example, where the object boundary overlaps with itself. At  $t = t_c$ , the object boundary loops around the two negative-sense roots and the positive-sense root in the same manner as Fig. 7(a). This example highlights that only altering flow strength is sufficient to cause a transition in the behavior of the dissolution process.

The transition in behavior is linked with the formation of the new roots in Fig. 9 as  $B$  is changed from 0 to  $-\frac{9}{10}$ . However, the middle panel of Fig. 10 for an intermediate flow strength of  $B = -\frac{33}{50}$  shows that this transition is more complicated. In this case, there is only a single negative-sense root in  $P$ . However, during time-evolution, the object boundary first overlaps with itself, and then the left loop shrinks to zero size, leading to a singular solution with an inverted cusp at time  $t = 0.1550602 < t_c$ .

We carried out a systematic sweep over the flow strengths over the range from  $B = 0$  to  $B = -1$ : initially the object collapses to a single point, at  $B \approx -0.233$  an inverted cusp forms, and at  $B \approx -0.794$  a second negative-sense root forms, when the left loop is large enough to persist until  $t_c$ . This result highlights that dissolution process can transition between at least three distinct behaviors. Furthermore, the result for  $B = -\frac{33}{50}$  shows that even if  $P$  only has a single negative-sense root, the dissolution process may not be straightforward, and may lead to an overlapping boundary or a singular solution.

Figure 11 shows which roots the generalized Newton–Raphson iteration will converge to, for the case of  $B = 0$ . The plot has an intricate structure and there are many small, distinct regions that converge to the central root. The denominator  $|P_z|^2 - |P_z|^2$  in Eq. (63) vanishes on a small loop surrounding the central root, and starting guesses near this loop are colored in darker shades, indicating that the root-finding algorithm takes many iterations to converge. The plot highlights the difficulty of finding the particular roots of interest in a general case.



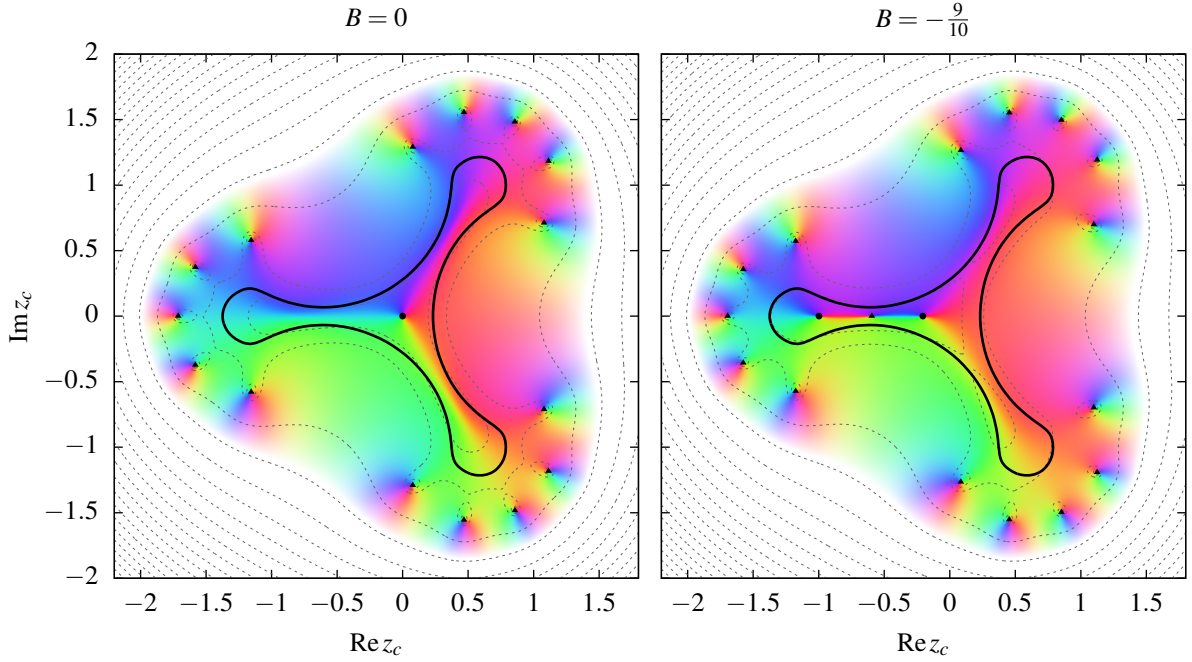


FIG. 9. Plot of the collapse point equation  $P(z_c)$  for the three-pronged object for (a)  $B = 0$ , and (b)  $B = -\frac{9}{10}$ . The colors correspond to the argument of  $P(z)$  using the same scale as Fig. 5. The positive-sense roots are shown with black triangles and the negative-sense roots are shown with black circles. The thick black line shows the boundary of the object. The thin dashed gray lines are contours of  $|P(z)|$  at  $\frac{1}{4}(n^4 + 1)$  for  $n \in \mathbb{N}_0$ .

## VII. CONCLUSION

In this paper, we studied a model of object dissolution within a two-dimensional potential flow, and we created a numerical implementation of it that allowed us to simulate the dissolution process for arbitrary objects described in terms of a Laurent series. The simulations revealed an exact relationship where the collapse point  $z_c$  is the root of a non-analytic function given in the terms of the Laurent coefficients and the flow strength. This relationship was subsequently derived analytically, but it is unlikely that it would have been discovered without the numerical results as a guide. These simulations made use of a high-order numerical method, and while these methods are often difficult or too computationally expensive to apply to real engineering problems, this work demonstrates their power in mathematical analysis: the numerical results for the collapse point are accurate enough to infer the underlying exact relationship with reasonable confidence. There are other examples where high-accuracy numerical methods have been used for similar purposes, such as demonstrating the existence of special solutions to equations [67, 68] or to discovering universal behavior [69].

The examples of Section VI create some interesting theoretical questions for future investigation. We expect that the first example of the pentagonal shape (Subsec. VIA) represents typical behavior for a broad class of objects, where the dissolution process is well-defined, the object collapses to a single point in finite time, and the collapse point function  $P(z_c)$  has a single negative-sense root. More specifically, we expect

this to be true for a large class of cases where the  $q_j$  are small in comparison to  $a$ , and hence the collapse point function in Eq. (58) will be dominated by the  $\bar{z}_c$  term and thus likely to have a single anti-analytic root close to the origin. However, the second example shows that not all cases may lead to this typical behavior, and object may dissolve into multiple fragments, with  $P(z_c)$  gaining additional negative-sense roots. The third example adds a further complication, showing that only a minor alteration of the flow strength  $B$  can lead to cases where dissolution is not well-defined, even though  $P(z_c)$  still has a single negative-sense root. The roots of  $P(z_c)$  are connected to the formation of the finite-time singularities, and give both an indication of the formation of local cusps, and potential global topological changes. The cusp formation is similar to continuous Laplacian growth [23, 29] although a key difference here is the breakage of symmetry due to the flow. This is particularly well illustrated by the third example, where the addition of flow breaks the three-fold symmetry and causes several transitions in behavior.

The collapse point results motivate two further questions: (A) what the conditions on the initial modes for  $P$  to have a single anti-analytic root, and (B) what are the conditions on the initial modes for the dissolution process to be well-defined and for the object to collapse to a single point? If questions A and B can be answered, then a further direction would be to identify a procedure capable of determining the collapse point with absolute certainty. The generalized Newton–Raphson method that was introduced in Subsec. VIA is very efficient at identifying roots, but it is difficult to determine *a priori* which

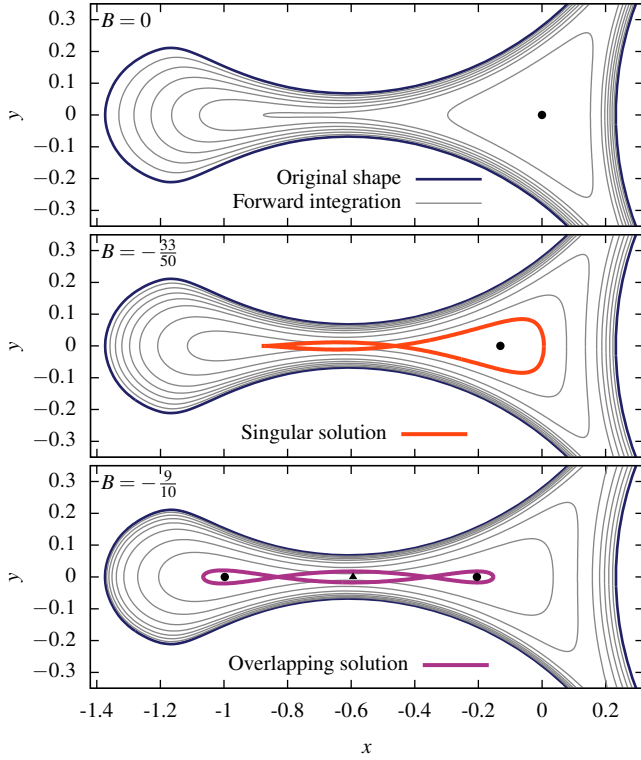


FIG. 10. Zoomed-in plot of the dissolution process for the three-pronged object, for three different values of the flow strength  $B$ , showing snapshots of the object boundary at intervals of  $\frac{t_c}{8}$  where  $t_c = 0.160885$ . The positive-sense roots are shown with black triangles and the negative-sense roots are shown with black circles. For  $B = 0$ , the object collapses to the origin at  $t = t_c$ . For  $B = -\frac{33}{50}$ , the object boundary overlaps and then a singular solution with a cusp forms at  $t = 0.1550602$ . For  $B = -\frac{9}{10}$  the boundary forms an overlapping curve at  $t = t_c$ .

root it will converge to, and plots of the convergence as a function of the starting guess exhibit a fractal structure as is typical for complex Newton–Raphson iterations. Furthermore, the non-analyticity of  $P(z_c)$  creates some difficulties whereby the total number of roots exhibits fundamentally different behavior than for analytic functions. An analytic cubic polynomial in  $z_c$  has exactly three roots (when counted with multiplicity) but the addition of a non-analytic  $\bar{z}_c$  as in the second example (Subsec. VIB) leads to seven roots, five of which are positive-sense and two of which are negative-sense. By using a winding argument, considering the curve  $P(Re^{i\theta})$  as  $R \rightarrow \infty$ , we obtain  $n_+ - n_- = N$  where  $N$  is the maximum non-zero mode, and  $n_{\pm}$  are the number of positive-sense and negative-sense roots. We also consider the Newton–Raphson fractals to be interesting in their own right, since they have a fundamentally different structure than typical Newton–Raphson fractals due to the one-dimensional set of points where the denominator in Eq. (63) vanishes. There is an interesting correspondence whereby each object has an associated fractal.

A variety of generalizations to the dissolution model could also be explored. The simple form of the right hand side of Eq. (11) was based on asymptotic considerations of the concen-

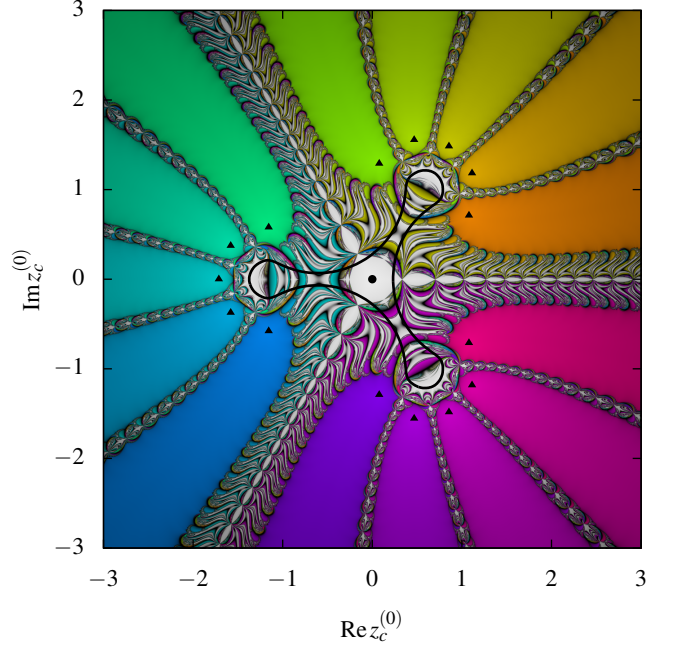


FIG. 11. Plot showing which root of the solution polynomial  $P$  a Newton–Raphson iteration will converge to when starting at  $z_c^{(0)}$ , for the three-pronged object when  $B = 0$ . The fifteen positive-sense roots of  $P$  are shown by black triangles, and the single negative-sense root at the origin is shown by a black circle. Each point is colored according to the argument of the root that it converges to, with the central root being shown in white. Darker shades show regions that require more iterations to converge.

tration profile in the low Péclet number limit, but the numerical method could be extended to more complex growth laws where higher powers of  $\cos \theta$  and  $\sin \theta$  are present. Since the derivation of the collapse point function is not highly dependent on the simple form of Eq. (11), it may be possible to generalize this to more complex growth laws as well. Another extension is to the case of regular polyhedral objects, which could be approximated using many terms in a Laurent series.

The second and third examples of Subsecs. VIB and VIC show that in some cases an object may dissolve into several components. In the current numerical method the dissolution process cannot be accurately simulated beyond the point where multiple fragments form, but it may be possible to extend the simulation to this case by using recent advances in conformal mapping for multiply connected domains [70–73]. The dissolution model is a particularly interesting example, since the physical process involves a single domain smoothly transitioning into two. We aim to investigate all of these interesting directions in future work.

Finally, we mention the discrete, stochastic analog of this problem. In the absence of advection, the diffusion-limited erosion of a surface leads to smooth, stable evolution that resembles the continuum limit of diffusion-limited dissolution [21, 35, 42, 43], but to our knowledge this model has never been analyzed (or even simulated) to the point where the last particle is removed. In the final stages of collapse,

discreteness must again become important. Of course, the same applies to advection–diffusion–limited dissolution, or any other conformally invariant dissolution model [38, 44]. We thus leave the reader with an open question: what is the probability that a given particle is the last to be removed by advection–diffusion–limited erosion of a finite cluster in a fluid flow?

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## Appendix A: Component form of the time-evolution equation

The numerical method introduced in Section III is based upon equating the different sine and cosine components of Eq. (14), which is

$$-1 + Ba \cos \theta = \text{Re} \left( \left[ ae^{-i\theta} - \sum_{n=0}^N n(b_n - ic_n)e^{in\theta} \right] \left[ ae^{i\theta} + \sum_{n=0}^N (\dot{b}_n + i\dot{c}_n)e^{-in\theta} \right] \right).$$

Multiplying out these power series yields

$$\begin{aligned} -1 + Ba \cos \theta = \text{Re} \left( a\dot{a} - \dot{a} \sum_{n=0}^N n(b_n - ic_n)e^{i(n+1)\theta} \right. \\ \left. + a \sum_{m=0}^N (\dot{b}_m + i\dot{c}_m)e^{i(m+1)\theta} \right. \\ \left. - \sum_{n=0}^N \sum_{m=0}^N n(b_n - ic_n)(\dot{b}_m + i\dot{c}_m)e^{i(n-m)\theta} \right). \end{aligned} \quad (\text{A1})$$

Taking the real component of the bracketed term yields

$$\begin{aligned} -1 + Ba \cos \theta = a\dot{a} - \sum_{n=0}^N \sum_{m=0}^N n \left[ (b_n \dot{b}_m + c_n \dot{c}_m) \cos(n-m)\theta \right. \\ \left. + (c_n \dot{b}_m - b_n \dot{c}_m) \sin(n-m)\theta \right] \\ + a \sum_{m=0}^N (\dot{b}_m \cos(m+1)\theta + \dot{c}_m \sin(m+1)\theta) \\ - \dot{a} \sum_{n=0}^N (b_n \cos(n+1)\theta + c_n \sin(n+1)\theta). \end{aligned} \quad (\text{A2})$$

Collecting terms with factors of sine and cosine yields

$$\begin{aligned} -1 + Ba \cos \theta = a\dot{a} - \sum_{n=0}^N n(b_n \dot{b}_n + c_n \dot{c}_n) \\ - \dot{a} \sum_{n=1}^{N+1} (n-1)(b_{n-1} \cos n\theta + c_{n-1} \sin n\theta) \\ + a \sum_{m=1}^{N+1} (\dot{b}_{m-1} \cos m\theta + \dot{c}_{m-1} \sin m\theta) \\ - \sum_{k=1}^N \sum_{m=0}^{N-k} \left[ (m+k)(b_{m+k} \dot{b}_m + c_{m+k} \dot{c}_m) \cos k\theta \right. \\ \left. + (m+k)(c_{m+k} \dot{b}_m - b_{m+k} \dot{c}_m) \sin k\theta \right. \\ \left. + m(b_m \dot{b}_{m+k} + c_m \dot{c}_{m+k}) \cos k\theta \right. \\ \left. - m(c_m \dot{b}_{m+k} - b_m \dot{c}_{m+k}) \sin k\theta \right]. \end{aligned} \quad (\text{A3})$$

Equating the terms with different factors of sine and cosine yields Eqs. (15), (16), (17), and (18), which together form the linear system that is used in the numerical integration method.

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